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^e MATHEMATICAL TABLES

CHIEFLY TO FOUR FIGURES

FIRST SERIES

BY

JAMES MILLS PEIRCE

UNIVERSITY PROFESSOR OF MATHEMATICS IN HARVARD
UNIVERSITY

BOSTON, U.S.A.:
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1891.

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Logarithms.

N	0	1	2	3	4	5	6	7	8	9	P. P. 1· 2· 3· 4· 5
10	0000	0043	0086	0128	0170	0212	0253	0294	0334	0374	4- 8-12-17-21
11	0414	0453	0492	0531	0569	0607	0645	0682	0719	0755	4 8-11-15-19
12	0792	0828	0864	0899	0934				1072		
13	1139	1173	1206	1239	1271	1303	1335	1367	1399	1430	3. 6.10.13.16
14	1461	1492	1523	1553	1584	1614	1644	1673	1703	1732	3. 6. 9.12.15
15	1761	1790	1818	1847	1875	1903	1931	1959	1987	2014	3. 6. 8.11.14
16	2041	2068	2095	2122	2148	2175	2201	2227	2253	2279	3. 5. 8.11 13
17						2430					
18					2648				2742		2.5.7.9.12
19	2788	2810	2833	2856	2878	2900	2923	2945	2967	2989	2. 4. 7. 9.11
20	3010	3032	3054	3075	3096	3118	3139	3160	3181	3201	2.4.6.811
21						3324					
22	3424	3444	3464	3483	3502	3522	3541	3560	3579	3598	2.4.6.8.10
28					3692				3766		
24	3802	3820	3838	3856	3874	3892	3909	3927	3945	3962	2.4.5.7.9
25	3979	3997	4014	4031	4048	4065	4082	4099	4116	4133	2 · 3 · 5 · 7 · 9
26	4150	4166	4183	4200	4216	4232	4249	4265	4281	4298	2 3 5 7 8
27	4314	4 330	4346	4362	4378	4393	4409	4425	4440	4456	2.3.5.6.8
28	4472	4487	4502	4518	4533	4548	4564	4579	4594	4609	2.3.5.6.8
29	4624	4639	4654	4669	4683	4698	4713	4728	4742	4757	1.3.4.6.7
30	4771	4786	4800	4814	4829	4843	4857	4871	4886	4900	1.3.4.6.7
31	4914	4928	4942	4955	4969	4983	4997	5011	5024	5038	1. 3. 4. 6. 7
32	5051	5065	5079	5092	5105	5119	5132	5145	5159	5172	1.3.4.5.7
33					5237				5289		1.3.4.5.6
34	5315	5328	5340	5358	5366	5378	5391	5403	5416	5428	1.3.4.5.6
35	5441	5 4 53	5465	5478	5490	5502	5.514	5527	5539	5551	1.2.4.5.6
36	5563	5575	5587	5599	5611	5623	5635	5647	5658	5670	1. 2. 4. 5. 6
37						5740	5752	5763	5775	5786	1 · 2 · 3 · 5 · 6
38					5843		5 866				1.2.3.5.6
39	5911	5922	5933	5944	5955	5966	5977	5988	5999	6010	1.2.3.4.6
40	6021	6031	6042	6053	6064	6075	6085	6096	6107	6117	1. 2. 3. 4. 5
41	6128	6138	6149	6160	6170	6180	6191	6201	6212	6222	1.2.3.4.5
42	6232	6243	6253	6263	6274	6284	6294	6304	6314	6325	1.2.3.4.5
43	6335	6345	6355	6365	6375	6385	6895	6405	6415	6425	1 · 2 · 3 · 4 · 5
44	6435	6444	6454	6464	6474	6484	6493	6503	6513	6522	1.2.3.4.5
45	6532	6542	6551	6561	6571	6580	6590	6599	6609	6618	1. 2. 3. 4. 5
46					6665				6702		
47	l .		6739						6794		
48	6812	6821	6830	6839	6848	6857	6866	6875	6884	6893	1. 2. 3. 4. 4
49	6902	6911	6920	6928	6937	6946	6955	6964	6972	6981	1.2.3.4.4
50	6990	6998	7007	7016	7024	7033	7042	7050	7059	7067	1.2.3.3.4
51			7093						7148		
/ 1	7180								7226		
/	243 7										1. 2. 2. 3. 4
											3 2. 2. 3.

												7 4
NT .	0	1	2	3	4	5	6	7	8 .	9	P. P.	
N	ľ	•	4	0	-	U	U	•	0	•	1. 2. 3. 4. 5	
55	7404	7410	7410	7497	7495	7449	7461	7450	7488	7474	1. 2. 2. 3. 4	
56											1. 2. 2. 3. 4	
57				7582							1. 2. 2. 3. 4	l
58											1. 1. 2. 3. 4	1
59				7731							1. 1. 2. 3. 4	
60	7782	7789	7796	7803	7810	7818	7825	7832	7889	7848	1. 1. 2. 3. 4	İ
61											1. 1. 2. 3. 4	1
62											1. 1. 2. 3. 3	ţ
63				8014							1. 1. 2. 3. 3	
64											1. 1. 2. 3. 3	
65	8129	8136	8142	8149	2156	8162	8169	8176	8182	8189	1. 1. 2. 3. 3	
66											1. 1. 2. 3. 3	l
67											1. 1. 2. 3. 3	
68				8344							1. 1. 2. 3. 3	1
69				8407							1. 1. 2. 3. 3	1
70	8451	8457	8463	8470	947R	8482	8488	8494	8500	8508	1. 1. 2. 2. 3	1
71											1. 1. 2. 2. 3	1
72				8591						8627		1
73				8651							1. 1. 2. 2. 3	ı
74											1. 1. 2. 2. 3	
75	9751	0758	9789	9789	9774	9770	0705	9701	9707	9909	1. 1. 2. 2. 3	l
76											1. 1. 2. 2. 3	
77											1. 1. 2. 2. 3	l
78				8938							1 1 2 2 3	1
79				8993							1 1 2 2 3	i
80	0031	0038	0042	9047	9059	9059	0083	9089	9074	9079	1. 1. 2. 2. 3	l
81											1. 1. 2. 2. 3	l
82											1. 1. 2. 2. 3	ı
83				9206							1. 1. 2. 2. 3	I
84				9258						9289		l
85	0004	0200	0904	0 200	0915	0300	0205	0000	0305	0340	1.1.2.2.3	
86											1. 1. 2. 2. 3	l
87											0. 1. 1. 2. 2	l
88				9460						9489		
89				9509							0. 1. 1. 2. 2	1
				-								
				9605						9633	0.1.1.2.2	ſ
91 92				9652							0. 1. 1. 2. 2 0. 1. 1. 2. 2	
93				9699						9727		1
94				9745						9773		1
												1
95											0· 1 1· 2· 2 0· 1· 1· 2· 2	
96 97						9890						1
98	9912	9917	9921	9926	9930	10034	1 9939	488 A	3 88 E	B BB	98 10 J · J · S	.5/
99	9958	9981	9985	9980	227	1 883	8 888 2000	88 88	81 89	98.T B.	888 0.1.1	5.5
00	5000	2001	3800	0008	0015	= 1 00 t	0 00		<u> </u>			

Logarithms.

N	0	1	2	3	4	5	6	7	8	9	10
100	0000	0004	0009	0013	0017	0022	0026	0030	0035	0039	0043
101	0043	0048	0052	0056	0060	0065	0069	0073	0077	0082	0086
102	0086	0090	0095	0099	0103	0107	0111	0116	0120	0124	0128
103	0128	0133	0137	0141	0145	0149	0154	0158	0162	0166	0170
104	0170	0175	0179	0183	0187	0191	0195	0199	0204	0208	0212
105	0212	0216	0220	0224	0228	0233	0237	0241	0245	0249	0253
106	0253	0257	0261	0265	0269		0278		0286		0294
107			0302	0306	0310		0318		0326		0334
108	0334	0338	0342	0346	0350	0354	0358	0362	0366	0370	0374
109	0374	0378	0382	0386	0390	0394	0398	0402	0406	0410	0414
110	0414	0418	0422	0426	0430	0434	0438	0441	0445	0449	0453
111	0453	0457	0461	0465	0469	0473	0477	0481	0484		0492
112	0492	0496	0500	0504		0512	0515		0523		0531
113	0531	0535	0538	0542	0546	0550	0554	0558	0561	0565	0569
114	0569	0573	0577	0580	0584	0588	0592	0596	0599	0603	0607
115	0607	0611	0615	0618	0622	0626	0630	0633	0637	0641	0645
116	0645			0656	0660	0663			0674		0682
117	0682	0686	0689	0693	0697	0700	0704		0711		0719
118	0719	0722	0726		0734		0741			0752	0755
119	0755	0759	0763	0766	0770	0774	0777	0781	0785	0788	0792
120	0792	0795	0799	0803	0806	0810	0813	0817	0821	0824	0828
121		0831	0835	0839	0842		0849	0853	0856		0864
122		0867			0878	0881		0888			0899
123	0899	0903	0906		0913	0917		0924			0984
124	0934	0938	0941	0945	0948	0952	0955	0959	0962	0966	0969
125	0969	0973	0976	0980	0983	0986	0990	0993	0997	1000	1004
126	1004	1007	1011	1014	1017	1021	1024	1028	1031	1035	1038
127	1038	1041	1045	1048	1052	1055	1059	1062	1065	1069	1072
128	1072	1075	1079	1082	1086	1089	1092	1096	1099	1103	1106
129	1106	1109	1113	1116	1119	1123	1126	1129	1133	1136	1139
130	1139	1143	1146	1149	1153	1156	1159	1163	1166	1169	1173
131		1176		1183	1186	1189	1193	1196	1199	1202	1206
132		1209			1219	1222		1229			1239
133		1242			1252	1255		1261		1268	1271
134	1271	1274	1278	1281	1284	1287	1290	1294	1297	1300	1303
135		1307			1316	1319		1326			1335
186		1339		1345	1348	1351		1358			1367
137	1367			1377	1380			1389			1399
138		1402			1411			1421			1430
139	1430	1433	1436	1440	1443	1446	1449	1452	1455	1458	1461
140			1467	1471	1474	1477		1483			1492
141	1492			1501	1504	1508		1514		1520	1523
142			1529		1535	1538		1544			1553
143		1556	1559	1562	1565	1569	1572	1575	1578	1581	1584
144	1584	1587	1590	1593	1696	1599	1602	1605	1608	1611	1614
145	1614	1617	1620	1623	1626	1629	1632		1638		1644
148		1647		1652	1655			1664		1670	1673
147	1673				1685					1700	
148	1 <i>703</i> .	170R	1708	1711	1714	1 1717	1720	1722	17726	1138	11133

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Logarithms.

						_						
N	0	1	2	3	4	5	6	7	8	9	10	
150	1781	1784	1787	1770	1772	1775	1778	1781	1784	1787	1790	
151				1798				1810		1816	1818	1
152	_			1827	-			1838			1847	
153				1855				1867			1875	ļ
154				1884				1895			1903	•
											1000	l
155				1912				1923			1931	
156				1940				1951			1959	l
157	1959	1962	1965	1967	1970	1973	1976	1978	1981	1984	1987	
158				1995		2000	2003	2006	2009	2011	2014	ł
159	2014	2017	2019	2022	2025	2028	2030	2033	2036	2038	2041	1
160	2041	2044	2047	2049	2052	2055	2057	2060	2063	2088	2068	1
161				2076				2087			2095	
162				2103				2114			2122	1
163				2130				2140			2148	1
164				2156				2167			2175	1
												1
165				2183				2193			2201	I
166				2209				2219			2227	1
167				2235				2245			2253	1
168				2261				2271			2279	ı
169	2279	2281	2284	2287	2289	2292	2294	2297	2299	2302	2304	ı
170	2304	2307	2310	2312	2315	2317	2320	2822	2325	2327	2330	ı
171	2330	2333	2335	2338	2340	2343	2345	2348	2350	2353	2355	
172	2355	2358	2360	2363	2365	2368	2370	2373	2375	2378	2380	1
173	2380	2383	2385	2388	2390	2393	2395	2398	2400	2403	2405	ı
174	2405	2408	2410	2413	2415	2418	2420	2423	2425	2428	2430	
175	2430	2493	2435	2438	2440	2443	2445	2448	2450	2453	2455	
176				2463				2472			2480	1
177				2487				2497			2504	ı
178				2512				2521			2529	1
179	2529	2531	2533	2536	2538	2541	2543	2545	2548	2550	2553	
180	0550	0555	0550	2560	05.00	05.05	05.07	2570	0570	0574	0577	ı
181				2584				2594			2577 2601	ı
182				2608				2617				ı
183				2632				2641			2625 2648	1
184		2651			2658		2662		2667		2672	1
104	_					_						1
185				2679				2688			2695	1
186				2702				2711			2718	1
187		2721			2728			2735			2742	1
188		2744			2751		2755		2760		2765	1
189	2765	2767	2769	2772	2774	2776	2778	2781	2783	2785	2788	
190	2788	2790	2792	2794	2797	2799	2801	2804	2806	2808	2810	ł
191	2810	2813	2815	2817	2819	2822	2824	2826	2828	2831	2833	1
192				2840		2844	2847			2853	2856	1
193				2862		2867	2869			2876	2878	ı
194	2878	2880	2882	2885	2887	2889	2891	2894	2896	2898	2900	1
195	2900	2903	2905	2907	2909	2911	2914	2916	2918	2920	2923	
196				2929		2934	2936	2938	2940	2242	2845	1
197		2947			2953	1 0050	00 50	0000	1 000	0 0'O'B	r 1 5.80.	1/1
198	2087	00.60	2071	0079	0075	1 000	ρ ρ ρ	U 502	ソン ひひ	84 F.	80100	101. 188
199	2989	2991	2993	2995	299	1 / 298	98 BB	05 30	04 3	008 3	nna I	=

Logarithms of Sums and Differences.

A	6.	7.	8.	9.	0.	1.	2.	3.
00	0.0000	0.0004	0.0043	0.0414 9	0.3010 50	1.0414 91	2.0043	3.0004
01	0.0000	0.0004	0.0044	0.0423 9	0.3061 51	1.0505 91	2.0142	3.0104
02	0.0000	0.0005	0.0045	0.0432 9	0.3111 51	1.0596 91	2.0241	3.0204
03	0.0000	0.0005	0.0046	0.0442 10	0.3163 52	1.0687 91	2.0340	3.0304
04	0.0000	0.0005	0.0047	0.0452 10	0.3215 52	1.0779 92	2.0439	3.0404
05	0.0000	0.0005	0.0048	0.0462 10	0.3267 53	1.0871 92	2.0539	3.0504
06	0.0000	0.0005	0.0050	0.0472 10	0.3321 53	1.0963 92	2.0638	3.0604
07	0.0001	0.0005	0.0051	0.0482 11	0.3374 54	1.1055 92	2.0737	3.0704
08	0.0001	0.0005	0.0052	0.0493 11	0.3429 55	1.1147 92	2.0836	3.0804
09	0.0001	0.0005	0.0053	0.0504 11	0.3484 55	1.1239 92	2.0935	3.0904
10	0.0001	0.0005	0.0054	0.0515 11	0.3539 56	1.1332 93	2.1034	3.1003
11	0.0001	0.0006	0.0056	0.0526 11	0.3595 56	1.1425 93	2.1134	3.1103
12	0.0001	0.0006	0.0057	0.0538 12	0.3652 57	1.1518 93	2.1233	3.1203
13	0.0001	0.0006	0.0058	0.0550 12	0.3709 57	1.1611 93	2.1332	3.1303
14	0.0001	0.0006	0.0060	0.0562 12	0.3766 58	1.1704 93	2.1431	3.1403
15	0.0001	0.0006	0.0061	0.0574 12	0.3825 59	1.1797 93	2.1531	3.1503
16	0.0001	0.0006	0.0062	0.0586 13	0.3884 59	1.1891 94	2.1630	3.1603
17	0.0001	0.0008	0.0064	0.0599 13	0.3943 60	1.1984 94	2.1729	3.1703
18	0.0001	0.0007	0.0065	0,0612 13	0.4003 60	1.2078 94	2.1829	3.1803
19	0.0001	0.0007	0.0067	0.0625 13	0.4063 61	1.2172 94	2.1928	3.1903
20	0.0001	0.0007	0.0068	0.0639 14	0.4124 61	1.2266 94	2.2027	3,2003
21	0.0001	0.0007	0.0070	0.0653 14	0.4186 62	1.2360 94	2.2127	3.2103
22	0.0001	0.0007	0.0071	0.0667 14	0.4248 62	1.2454 94	2.2226	3.2203
23	0.0001	0.0007	0.0073	0.0681 15	0.4311 63	1.2548 94	2.2325	3.2303
24	0.0001	0.0008	0.0075	0.0696 15	0.4374 63	1.2643 95	2.2425	3.2402
25	0.0001	0.0008	0.0077	0.0711 15	0.4438 64	1.2738 95	2.2524	3.2502
26	0.0001	0.0008	0.0078	0.0726 15	0.4502 65	1.2832 95	2.2624	3.2602
27	0.0001	0.0008	0.0080	0.0742 16	0.4567 65	1.2927 95	2.2723	3.2702
28	0.0001	0.0008	0.0082	0.0757 16	0.4632 66	1.3022 95	2.2823	3.2802
29	0.0001	0.0008	0.0084	0.0774 16	0.4698 66	1.3117 95	2.2922	3.2902
30	0.0001	0.0009	0.0086	0.0790 17	0.4764 67	1.3212 95	2.3022	3,3002
31	0.0001	0.0009	0.0088	0.0807 17	0.4831 67	1.3308 95	2.3121	3.3102
32	0.0001	0.0009	0.0090	0.0824 17	0.4899 68	1.3403 95	2.3221	3.3202
33	0.0001	0.0009	0.0092	0.0841 18	0.4966 68	1.3499 96	2.3320	3.3302
34	0.0001	0.0009	0.0094	0.0859 18	0.5035 69	1.3594 96	2.3420	3.3402
35	0.0001	0.0010	0.0096	0.0877 18	0.5104 69	1.3690 96	2.3519	3.3502
36	0.0001	0.0010	0.0098	0.0896 19	0.5173 70	1.3786 96	2.3619	3.3602
37	0.0001	0.0010	0.0101	0.0915 19	0.5243 70	1.3881 96	2.3718	3.3702
38	0.0001	0.0010	0.0103	0.0934 19	0.5313 71	1.3977 96	2.3818	3.3802
39	0.0001	0.0011	0.0105	0.0953 20	0.5384 71	1.4073 96	2.3918	3.3902
40	0.0001	0.0011	0.0108	0.0973 20	0.5455 72	1.4170 96	2.4017	3.4002
41	0.0001	0.0011	0.0110	0.0993 20	0.5527 72	1.4266 96	2.4117	3.4102
42	0.0001	0.0011	0.0113	0.1014 21	0.5599 72	1.4362 96	2.4216	3.4202
43	0.0001	0.0012	0.0115	0.1035 21	0.5672 73	1.4458 96	2.4316	3.4302
44	0.0001	0.0012	0.0118	0.1057 22	0.5745 73	1.4555 96	2.4416	3.4402
45	0.0001	0.0012	0.0121	0.1078 22	0.5819 74	1.4651 97	2.4515	3.4502
46	0.0001	0.0013	0.0123	0.1101 22	0.5893 74	1.4748 97	2.4615	3.4602
47	0.0001	0.0013	0.0126	0.1123 23	0.5967 75	1.4845 97	2.4715	3.4701
48	0.0001	0.0013	0.0129	0.1146 23	0.6042 75	1.4941 97	2.4814	3.4801
19 C	0.0001 /	0.0013	0.0132	0.1169 24	0.6118 76	1.5038 gr	\ 2.4914	¹ 3.4901

Logarithms of Sums and Differences.

A	6.	7.	8.	9.	0.	1.	2. .	3.
50	0.0001	0.0014	0.0135	0.1193 24	0.6193 76	1.5135 97	2.5014	3.5001
51	0.0001	0.0014	0.0138	0.1218 24	0.6269 76	1.5232 97	2.5113	3.5101
52	0.0001	0.0014	0.0141	0.1242 25	0.634677	1.5329 97	2.5213	3.5201
53	0.0001	0.0015	0.0145	0.1267 25	0.6423 77	1.5426 97	2.5313	3.5301
54	0.0002	0.0015	0.0148	0.1293 26	0.6501 78	1.5523 97	2.5413	3.5401
55	0.0002	0.0015	0.0151	0.1319 26	0.6578 78	1.5621 97	2.5512	3.5501
56 57	0.0002	0.0016	0.0155	0.1345 27	0.6657 78	1.5718 97	2.5612	3.5601
58	0.0002 0.0002	0.0016 0.0016	0.0158 0.0162	0.1372 27 0.1399 28	0.6735 79 0.6814 79	1.5815 97 1.5913 97	2.5712 2.5811	3.5701 3.5801
59	0.0002	0.0017	0.0166	0.1427 28	0.6893 80	1.6010 97	2.5911	3.5901
60	0.0002	0.0017	0.0170	0.1455 28	0.6973 80	1.6108 98	2.6011	3.6001
61	0.0002	0.0017	0.0173	0.1484 29	0.7053 80	1.6205 98	2.6111	3.6101
62	0.0002	0.0018	0.0177	0.1513 29	0,7134 81	1.6303 98	2.6210	3.6201
63	0.0002	0.0018	0.0181	0.1543 30	0.7215 81	1.6401 98	2.6310	3.6301
64	0.0002	0.0019	0.0186	0.1573 30	0,7296 81	1.6498 98	2.6410	3.6401
65	0.0002	0.0019	0.0190	0.1604 31	0,7377 82	1.6596 98	2.6510	3.6501
66	0.0002	0.0020	0.0194	0.1635 31	0.7459 82	1.6694 98	2.6609	3.6601
67	0.0002	0.0020	0.0199	0.1666 32	0.7541 82	1.6792 98	2.6709	3.6701
68	0.0002	0.0021	0.0203	0.1699 32	0.7624 83	1.6890 98	2.6809	3.6801
69	0.0002	0.0021	0.0208	0.1731 33	0,7707 83	1.6988 98	2.6909	3.6901
70	0.0002	0.0022	0.0212	0.1764 33	0,7790 83	1.7086 98	2.7009	3.7001
71	0.0002	0.0022	0.0217	0.1798 34	0.7874 84	1.7184 98	2.7108	3.7101
72 73	0.0002 0.0002	0.0023	0.0222 0.0227	0.1832 34 0.1867 35	0.7957 84	1.7282 98 1.7380 98	2.7208 2.7308	3.7201 3.7301
74	0.0002	0.0023	0.0232	0.1902 35	0.8126 85	1.7478 98	2.7408	3.7401
75	0.0002	0.0024	0.0238	0.1938 36	0.8211 85	1.7577 98	2.7508	3.7501
76	0.0002	0.0024	0.0238	0.1974 37	0.8211 85	1.7675 98	2.7608	3.7801
77	0.0003	0.0025	0.0248	0.2011 37	0.8381 85	1.7773 98	2.7707	3.7701
78	0.0003	0.0026	0.0254	0.2048 38	0.8467 86	1.7871 98	2.7807	3.7801
79	0.0003	0.0027	0.0260	0.2086 38	0.8553 86	1.7970 98	2.7907	3.7901
80	0.0003	0.0027	0.0266	0.2124 39	0.8639 86	1.8068 98	2.8007	3.8001
81	0.0003	0.0028	0.0272	0.2163 39	0.8725 87	1.8167 98	2.8107	3.8101
82	0.0003	0.0029	0.0278	0.2203 40	0,8812 87	1.8265 99	2.8207	3.8201
83	0.0003	0.0029	0.0284	0.2243 40	0.8899 87	1.8364 99	2.8306	3.8301
84	0.0003	0.0030	0.0291	0.2284 41	0.8986 87	1.8462 99	2.8406	3.8401
85	0.0003	0.0031	0.0297	0.2325 41	0.9074 88	1.8561 99	2.8506	3.8501
86	0.0003	0.0031	0.0304	0.2366 42	0.916288	1.8660 99	2.8606	3.8601
87 88	0.0003	0.0032	0.0311	0.2409 43 0.2452 43	0.9250 88 0.9338 88	1.8758 99 1.8857 99	2.8706 2.8806	3.8701 3.8801
89	0.0003	0.0033	0.0318	0.2495 44	0,9426 89	1.8956 99	2.8906	3.8901
							2.9005	3.9001
90 91	0.0003 0.0004	0.0034	0.0332 0.0339	0.2539 44 0.2584 45	0.9515 89 0.9604 89	1.9054 99 1.9153 99	2.9105	3.9101
92	0.0004	0.0036	0.0338	0.2629 45	0.9693 89	1.9252 99	2.9205	3.9201
93	0.0004	0.0037	0.0355	0.2674 46	0.9782 89	1.9351 99	2.9305	3.9301
94	0.0004	0.0038	0.0363	0.2721 47	0.9872 90	1.9450 99	2.9405	3.9400
95	0.0004	0.0039	0.0371	0.2767 47	0.9962 90	1.9548 99	2.9505	3.9500
96	0.0004	0.0039	0.0379	0.2815 48	1.0052 90	1.9647 99	2.9605	3.9600
97	0.0004	0.0040	0.0387	0.286348	1.0142 90	1.9746 99	2.9705	
98	0.0004	0.0041	0.0396	0.2911 49	1.0333 21	1.9845 99 1 1.9944 9	7088,8/ 2000	0080.E/a
99	0.0004	0.0042	0.0405	0,2961 49	1.0383 0	91 \ 2.004	100,0	3.50

φ	0° lsin ltn	l sc	1º lsin ltn	lsc	2º lsin ltn	l sc	
00/	- ∞	00	8.2419 19 72	01	8.5428 31 36	03	60′
01' 02' 03'	6.4637 37 6.7648 48 6.9408 08 7.0658 58	00 00 00	8.2490 91 71 8.2561 62 70 8.2630 31 69 8.2699*00 68	01 01 01	8.5464 67 36 8.5500 03 36 8.5535 38 35 8.5571 73 35	03 03 03 03	59' 58' 57' 56'
04/ 05/ 06/	7.1627 27	00 00	8.2766 67 67	01 01 01	8.5605 08 35	03	55′ 54′
07' 08' 09'	7.2419 19 7.3088 88 7.3668 68 7.4180 80	00 00 00	8.2832 33 66 8.2898 99 65 8.2962 63 64 8.3025 26 63	01 01 01	8.5640 43 34 8.5674 77 34 8.5708 11 34 8.5742 45 34	03 03 03 03	53' 52' 51'
10′	7.4637 37	00	8.3088 89 62	01	8.5776 79 33	03	50′
11' 12' 13' 14'	7.5051 51 7.5429 29 7.5777 77 7.8099 99	00 00 00	8.3150 50 61 8.3210 11 60 8.3270 71 59 8.3329 30 59	01 01 01 01	8.5809 12 33 8.5842 45 33 8.5875 78 33 8.5907 11 32	03 03 03 03	49' 48' 47' 46'
15′	7.6398 98	00	8.3388 89 58	01	8.5939 43 32	03	45′
16' 17' 18' 19'	7.6678 78 7.6942 42 7.7190 90 7.7425 25	00 00 00	8.3445 46 57 8.3502 03 56 8.3558 59 56 8.3613 14 55	01 01 01 01	8.5972 75 32 8.6003 07 32 8.6035 38 31 8.6066 70 31	03 03 04 04	44' 43' 42' 41'
20′	7.7648 48	00	8.3668 69 54	01	8.6097*01 31	04	40′
21' 22' 23' 24'	7.7859 60 7.8061 62 7.8255 55 7.8439 39	00 00 00	8.3722 23 54 8.3775 76 53 8.3828 29 52 8.3880 81 52	01 01 01 01	8.6128 32 31 8.6159 63 31 8.6189 93 30 8.6220 23 30	04 04 04 04	39' 38' 37' 36'
25	7.8617 17	00	8.3931 32 51	01	8.6250 54 30	04	35′
26' 27' 28' 29'	7.8787 87 7.8951 51 7.9109 09 7.9261 61	00 00 00	8.3982 83 51 8.4032 33 50 8.4082 83 49 8.4131 32 49	01 01 01 01	8.6279 83 30 8.6309 13 30 8.6339 43 29 8.6368 72 29	04 04 04 04	34/ 33/ 32/ 31/
30′	7.9408 09 ·	00	8.4179 81 48	01	8.6397*01 29	04	30 ′
31/ 32/ 33/ 34/	7.9651 51 7.9689 89 7.9822 23 132 7.9952 52 128	00 00 00	8.4227 29 48 8.4275 76 47 8.4322 23 47 8.4368 70 46	02 02 02 02	8.6426 30 29 8.6454 59 29 8.6483 87 28 8.6511 15 28	04 04 04 04	29' 28' 27' 26'
35′	8.0078 78 124	00	8.4414 16 46	02	8.6539 44 28	04	25′
36' 37' 38' 39'	8.0200 00 121 8.0319 19 117 8.0435 35 114 8.0548 48 111	00 00 00	8.4459 61 45 8.4504 06 45 8.4549 51 44 8.4593 95 44	02 02 02 02	8.6567 71 28 8.6596 99 28 8.6622 27 27 8.6650 54 27	04 05 05 05	24/ 23/ 22/ 21/
40′	8.0658 58 109	00	8.4637 38 43	02	8.6677 82 27	05	20′
41' 42' 43' 44'	8.0765 65 106 8.0870 70 103 8.0972 72 101 8.1072 72 99	00 00 00 00	8.4680 82 43 8.4723 25 43 8.4765 67 42 8.4807 09 42	02 02 02 02	8.6704 09 27 8.6731 36 27 8.6758 62 27 8.6784 89 26	05 05 05 05	19' 18' 17' 16'
45′	8.1169 70 97	00	8.4848 51 41	02	8.6810 15 26	05	15′
46' 47' 48' 49'	8.1265 65 94 8.1358 59 92 8.1450 50 90 8.1539 40 89	00 00 00	8.4890 92 41 8.4930 33 41 8.4971 73 40 8.5011 13 40	02 02 02 02	8.6837 42 26 8.6863 68 26 8.6889 94 26 8.6914 20 26	05 05 05 05	14/ 13/ 12/ 11/
50′	8.1627 27 87	00	8.5050 53 39	02	8.6940 45 26	05	10′
51' 52' 53' 54'	8.1713 13 85 8.1797 98 84 8.1880 80 82 8.1961 62 80	00 00 01 01	8.5090 92 39 8.5129 31 39 8.5167 70 38 8.5206 08 38	02 02 02 02	8.6965 71 25 8.6991 96 25 8.7016 21 25 8.7041 46 25	05 05 06 06	09' 08' 07' 06'
55′	8.2041 41 79	01	8.5243 46 38	02	8.7066 71 25	06	05′
56' 57' 58' 59'	8.2119 20 78 8.2196 96 76 8.2271 72 75 8.2346 46 74	01 01 01 01	8.5281 83 37 8.5318 21 37 8.5355 58 37 8.5392 94 37	02 03 03 03	8.7090 96 25 8.7115 21 25 8.7140 45 24 8.7164 70 24	06 06 06 0 0	04' 03' 02' 01'
<i>BO'</i>	8.2419 19 72	01	8.5428 31 36	03	8.7188 94 24	108	100
/8	9º leos letn le	esc	88° lcos lctn	l esc	87° I cos I ctn	J GB	θ [ε

φ	3° lsin ltn	lsc	4° lsin ltn	l sc	5° lsin ltn la	se
00'	8.7188 94 24	06	8.8436 46 18	11		7 60′
01' 02' 03' 04'	8.7212 18 24 8.7236 42 24 8.7260 66 24 8.7283 90 24	06 06 06 06	8.8454 65 18 8.8472 83 18 8.8490*01 18 8.8500 18 18	11 11 11 11	8.9417 34 14 1 8.9432 49 14 1 8.9446 63 14 1 8.9460 77 14 1	7 59' 7 58' 7 57' 7 56'
05 [/]	8.7307 13 23	06 06	8.8525 36 18	11	8.9475 92 14 1	7 55
07' 08' 09'	8.7330 37 23 8.7354 60 23 8.7377 83 23 8.7400 06 23	06 06 07	8.8543 54 18 8.8560 72 18 8.8578 89 18 8.8595*07 17	;; ;;	8.9489*06 14 1 8.9503 20 14 1 8.9517 34 14 1 8.9531 49 14 1	7 54/ 7 53/ 7 52/ 8 51/
10′	8.7423 29 23	07	8.8613 24 17	11	8.9545 63 14 1	8 50/
11' 12' 13' 14'	8.7445 52 23 8.7468 75 23 8.7491 97 23 8.7513 20 22	07 07 07 07	8.8630 42 17 8.8647 59 17 8.8665 76 17 8.8682 94 17	12 12 12 12 12	8.9573 91 14 1 8.9587*05 14 1	8 49' 8 48' 8 47' 8 46'
15	8.7 535 42 22	07	8.8699*11 17	12	8.9614 33 14 1	8 45/
16' 17' 18' 19'	8.7557 65 22 8.7580 87 22 8.7602 09 22 8.7623 31 22	07 07 07 07	8.8716 28 17 8.8733 45 17 8.8749 62 17 8.8766 78 17	12 12 12 12	8.9642 60 14 1 8.9655 74 14 1	8 44/ 8 43/ 9 42/ 9 41/
20′	8.7645 52 22	07	8.8783 95 17	12		9 40'
21' 22' 23' 24'	8.7667 74 22 8.7688 96 22 8.7710 17 21 8.7731 39 21	07 08 08 08	8.8799*12 17 8.8816 29 17 8.8833 45 17 8.8849 62 16	13 13 13 13	8.9709 29 14 1 8.9723 42 13 1	9 39/ 9 38/ 9 37/ 9 36/
25	8.7752 60 21	08	8.8865 78 16	13		9 35′
267' 277' 289'	8.7773 81 21 8.7794*02 21 8.7815 23 21 8.7836 44 21	08 08 08 08	8.8882 95 16 8.8898*11 16 8.8914 27 16 8.8930 44 16	13 13 13 13	8.9763 82 13 2 8.9776 96 13 2 8.9789*09 13 2 8.9803 23 13 2	0 34/ 0 33/ 0 32/ 0 31/
30'	8.7857 65 21	08	8.8946 60 16	13		0 30/
31/ 32/ 33/ 34/	8.7877 86 21 8.7898*06 20 8.7918 27 20 8.7939 47 20	08 08 08 08	8.8962 76 16 8.8978 92 16 8.8994*08 16 8.9010 24 16	14 14 14 14	8.9829 49 13 2 8.9842 62 13 2 8.9855 75 13 2 8.9868 88 13 2	0 29' 0 28' 0 27' 1 26'
35′	8.7959 67 20	08	8.9026 40 16	14		1 25/
36' 37' 38' 39'	8.7979 88 20 8.7999*08 20 8.8019 28 20 8.8039 48 20	09 09 09 09	8.9042 56 16 8.9057 71 16 8.9073 87 16 8.9089*03 16	14 14 14 14	8.9894*15 13 2 8.9907 28 13 2 8.9919 40 13 2 8.9932 53 13 2	1 24/ 1 23/ 1 22/ 1 21/
40′	8.8059 67 20	09	8.9104 18 16	14	8.9945 66 13 2	—1 11
41' 42' 43' 44'	8.8078 87 20 8.8098*07 20 8.8117 26 19 8.8137 46 19	09 09 09 09	8.9119 34 15 8.9135 50 15 8.9150 65 15 8.9166 80 15	15 15 15 15	8.9983*05 13 2	1 19' 18' 2 17' 2 16'
45/	8.8156 65 19	09	8.9181 96 15	15		2 15/
46' 47' 48' 49'	8.8175 85 19 8.8194*04 19 8.8213 23 19 8.8232 42 19	09 09 10 10	8.9196*11 15 8.9211 26 15 8.9226 41 15 8.9241 56 15	15 15 16 15	9.0021 43 13 2 9.0033 55 13 2 9.0046 68 12 2 9.0058 80 12 2	2 14/ 2 13/ 2 12/ 2 11/
50/	8.8251 61 19	10	8.9256 72 15	15	9.0070 93 12 2	3 10′
51' 52' 53' 54'	8.8270 80 19 8.8289 99 19 8.8307 17 19 8.8326 36 19	10 10 10 10	8.9271 87 15 8.9286*02 15 8.9301 16 15 8.9315 31 15	16 16 16 16	9.0083*05 12 2 9.0095*18 12 2 9.0107 30 12 2 9.0120 43 12 2	3 09/ 3 08/ 3 07/ 3 06/
55′	8.834 5 55 19	10	8.9330 46 15	16		3 05/
56' 57' 58' 59'	8.8363 73 18 8.8381 92 18 8.8400 10 18 8.8418 28 18	10 10 10 11	8.9345 61 15 8.9359 76 15 8.9374 90 15 8.9388*05 15	16 16 16 16	9.0144 67 12 2 9.0156 80 12 2 9.0168 92 12 2 9.0180 04 12	3 047 4 087 24 087
60'	8.8436 46 18	11	8.9403 20 14	1/2	8.0188-18 12	184 00.
	86º lcos lctn	CSC	85° lcos lctn	Je	84° 1 cos 1 ctr	1 686

Logarithms of Circular Functions.

ф	S lsin φ	φ	Tlta	nφ	ϕ lsec ϕ	φ	l sec φ
ļ	6.46		6.46	\dashv	0.00		0.00
0°00′.000		0°00′.	000 -	∞ 0°	00/.000	4°20	Y.701
li	37 I	0°44′	155 37 8.1	087 0 º	52',164 00	4°30	V.918 13
1°51 ′.4 79	36 8.5108	1°40′.		663 l ₁ °	30'.348 01	4°40	V.762 14
2°49′.567	8.6929	2°15′.		948 10	56'.634 ^{UZ}	4°50	7.271 15
3°82′.318	35 8,7904	2°42′.	000 41 000	751 _{2°}	17/.998 03	4°58	7.477 16
	34	3°05′.	909 40 911	336	36'.469 ⁰⁴		7.407 17
4°07′.789	8. 8 57 4	3°26′.	171 40 01	180 º°	52/.976 05		7.084 18
4°38′.783	8.9085	3°45′.	001 1 010	1,0	08'.038 06		7.528 19
E000/ 050	32	4°02′. 4°19′.	904 7 9.0	000	21'.977	_	7.758 20
5°06′.659	8.9498 31	4°34′.	111 40 010		35'.016 08		7.789 21
5°32′.201	8.9845	4°48′.			47/300 09	_	7.633 22
5°55′.913	9.0143	5°02′.			58'.955 10		7.805 23
l	29	5°15′.	780 ⁴⁹ 8.9	040			~ ~ 1
6°18′.138	9.0405	5°28′.	401 50 8.9	915	10'.064 12		1.01# OF
li		5°40′.		973 ^{4°}	20′.701 12	0.17	1.170 ²⁵
		5°52′.		121			
		6°03′.	623 ⁵³ 9.0	260			1
φ	l sin ϕ	$l \csc \phi$	l tan ϕ	l ctn φ	lsec φ lc	08 φ	
6° 00′	9.0192 120 (0.9808	9.0216 122	0.9784	0.0024 1 9.9	976	84° 00′
6° 10′	9.0311 117 (9,0336 118		0.0025 1 9.9		83° 50′
6° 20′	9,0426 114 (9.0453 115		0.0027 1 9.9		83° 40′
6° 30′	9.0539 111 (9.0567 112		0.0028 1 9.8		83° 30′
6° 40′	9.0648 108 (9.0678 110		0.0029 1 9.9		83° 20′
6° 50′	9.0755 105 (J.8240	9.0786 107	0.9314	0.0031 2 9.9	9969	83° 10′
79 00'	9,0859 103 (0.9141	9.0891 104	0.9109	0.0032 2 9.9	968	83° 00′
7° 10′	9.0961 100 (0.9039	9.0995 102	0.9005	0.0034 2 9.9	9966	82° 50′
7° 20′	9.1060 98 (0.8940	9.1096 100	0.8904	0.0036 2 9.8	964	82° 40′
7° 30′		0.8843		0.8806	0.0037 2 9.8		82° 30′
7° 40′		0.8748		0.8709	0.0039 2 9.9		82° 20′
7° 60′	9.1345 92 (0.8655	9.1385 94	0.8615	0.0041 2 9.9	959	82° 10′
8° 00′	9.1436 90 (0.8564	9.1478 92	0.8522	0.0042 2 9.8	958	82° 00′
8° 10′		0.8475		0.8431	0.0044 2 9.8		81° 50′
8° 20′		0.8388		0.8342	0.0046 2 9.8		81° 40′
8° 30′		0.8303		0.8255	0.0048 2 9.9		81° 30′
8° 40′		0.8219		0.8169	0.0050 2 9.9		81° 20′
8° 50′	9.1863 81 (0.8137	9.1915 83	0.8085	0.0052 2 9.8	9448	81° 10′
9° 00′	9.1943 80 (0.8 0 57		0.8003	0.0054 2 9.9		81°00′
9° 10′		0.7978		0.7922	0.0056 2 9.9		80° 50′
9° 20′		0.7900		0.7842	0.0058 2 9.8		80° 40′
9° 30′		0.7824		0.7764	0.0060 2 9.1		80° 30′
9° 40′		0.7749		0.7687	0.0062 2 9.8		80° 20′
9° 50′	9.2324 73 (0.7676	9.2389 75	0.7611	0.0064 2 9.5	9836	80° 10′
10000	9.2397 72	0.7603	9.2463 74	0.7537	0.0066 2 9.1	9934	80° 00′
	$l\cos\theta$ 1	sec 0	letn θ	l tan θ	l csc 0 l	0 ais	θ

ø	lsinφ lcscφ	ltanφ lctnφ	l sec φ l cos φ.	
10° 00′	9.2397 72 0.7603	9.2463 74 0.7537	0.0066 2 9.9934	80° 00′
10° 10′ 10° 20′ 10° 30′ 10° 40′ 10° 50′	9.2468 70 0.7532 9.2538 69 0.7462 9.2606 68 0.7394 9.2674 67 0.7326 9.2740 66 0.7260	9,2536 73 0.7464 9,2609 72 0.7391 9,2680 71 0.7320 9,2750 69 0.7250 9,2819 68 0.7181	0.0069 2 9.9931 0.0071 2 9.9929 0.0073 2 9.9927 0.0076 2 9.9924 0.0078 2 9.9922	79° 50′ 79° 40′ 79° 30′ 79° 20′ 79° 10′
11° 00′	9.2806 65 0.7194	9.2887 67 0.7113	0.0081 2 9.9919	79° 00′
11° 10′ 11° 20′ 11° 30′ 11° 40′ 11° 50′	9.2870 64 0.7130 9.2934 63 0.7066 9.2997 62 0.7003 9.3058 61 0.6942 9.3119 60 0.6881	9.2953 66 0.7047 9.3020 66 0.6980 9.3085 65 0.6915 9.3149 64 0.6851 9.3212 63 0.6788	0.0083 2 9.9917 0.0086 3 9.9914 0.0088 3 9.9912 0.0091 3 9.9909 0.0093 3 9.9907	78° 50′ 78° 40′ 78° 30′ 78° 20′ 78° 10′
12° 00′	9.3179 59 0.6821	9.3275 62 0.6725	0.0096 3 9.9904	78° 00′
12° 10′ 12° 20′ 12° 30′ 12° 40′ 12° 50′	9.3238 59 0.6762 9.3296 58 0.6704 9.3353 57 0.6647 9.3410 56 0.6590 9.3466 55 0.6534	9.3336 61 0.6664 9.3397 61 0.6603 9.3458 60 0.6542 9.3517 59 0.6483 9.3576 58 0.6424	0.0101 3 9.9899 0.0104 3 9.9896 0.0107 3 9.9893	77° 50′ 77° 40′ 77° 30′ 77° 20′ 77° 10′
18° 00′	9.3521 55 0.6479	9.3634 58 0.6366	0.0113 3 9.9887	77° 00′
13° 10′ 13° 20′ 13° 30′ 13° 40′ 13° 50′	9.3575 54 0.6425 9.3629 53 0.6371 9.3682 53 0.6318 9.3734 52 0.6266 9.3786 51 0.6214	9.3691 57 0.6309 9.3748 56 0.6252 9.3804 56 0.6196 9.3859 55 0.6141 9.3914 54 0.6086	0.0116 3 9.9884 0.0119 3 9.9881 0.0122 3 9.9878 0.0125 3 9.9875 0.0128 3 9.9872	76° 50′ 76° 40′ 76° 30′ 76° 20′ 76° 10′
14° 00′	9.3837 51 0.6163	9.3968 54 0.6032	0.0131 3 9.9869	76° 00′
14° 10′ 14° 20′ 14° 30′ 14° 40′ 14° 50′	9.3887 50 0.6113 9.3937 49 0.6063 9.3986 49 0.6014 9.4035 48 0.5965 9.4083 48 0.5917	9.4074 53 0.5926	0.0137 3 9.9863	75° 50′ 75° 40′ 75° 30′ 75° 20′ 75° 10′
15° 00′	9.4130 47 0.5870	9.4281 51 Q.5719	0.0151 3 9.9849	75° 00′
15° 10′ 15° 20′ 15° 30′ 15° 40′ 15° 50′	9.4177 47 0.5823 9.4223 46 0.5777 9.4269 46 0.5731 9.4314 45 0.5686 9.4359 45 0.5641	9.4331 50 0.5669 9.4381 50 0.5619 9.4430 49 0.5570 9.4479 49 0.5521 9.4527 48 0.5473	0.0154 3 9.9846 0.0157 3 9.9843 0.0161 4 9.9839 0.0164 4 9.9836 0.0168 4 9.9832	74° 50′ 74° 40′ 74° 30′ 74° 20′ 74° 10′
16° 00′	9.4403 44 0.5597	9.4575 48 0.5425	0.0172 4 9.9828	74° 00′
16° 10′ 16° 20′ 16° 30′ 16° 40′ 16° 50′	9.4447 44 0.5553 9.4491 43 0.5509 9.4533 43 0.5467 9.4576 42 0.5424 9.4618 42 0.5382 9.4659 41 0.5341	9.4622 47 0.5378 9.4669 47 0.5331 9.4716 46 0.5284 9.4762 46 0.5238 9.4808 46 0.5192 9.4853 45 0.5147	0.0186 4 9.9814 0.0190 4 9.9810	73° 50′ 73° 40′ 73° 30′ 73° 20′ 73° 10′ 78° 00 ′
	lcos θ l sec θ	letn 0 ltan 0	lesc 0 lsin	.0 9

>9:5

11

Logarithms of Circular Functions.

φ	lsinφ lese φ	ltanφ lctnφ	l sec φ l cos φ	
17° 00′	9.4659 41 0.5341	9.4853 45 0.5147	0.0194 4 9.9806	73° 00′
17° 10′	9.4700 41 0.5300	9.4898 45 0.5102	0.0198 4 9.9802	72° 50′
17° 20′	9.4741 40 0.5259		0.0202 4 9.9798	72° 40′
17° 30′ 17° 40′	9.4781 40 0.5219	9.4987 44 0.5013	0.0206 4 9.9794	72° 30′ 72° 20′
17° 50′	9.4821 40 0.5179 9.4861 39 0.5139	9.5031 44 0.4969 9.5075 43 0.4925	0.0210 4 9.9790 0.0214 4 9.9786	72° 20'
				1
18° 00′	9.4900 39 0.5100		0.0218 4 9.9782	72° 00′
18° 10′	9.4939 38 0.5061	9.5161 43 0.4839	0.0222 4 9.9778	71° 50′
18° 20′	9.4977 38 0.5023	9.5203 42 0.4797	0.0226 4 9.9774	71° 40′
18° 30′ 18° 40′	9.5015 38 0.4985	9.5245 42 0.4755	0.0230 4 9.9770	71° 30′ 71° 20′
18° 50′	9.5052 37 0.4948 9.5090 37 0 4910		0.0235 4 9.9765	71° 20′ 71° 10′
1			0.0239 4 9.9761	71 10
19° 00′	9.5126 37 0.4874		0.0243 4 9.9757	71° 00′
19° 10′	9.5163 36 0.4837		0.0248 4 9.9752	70° 50′
19° 20′	9.5199 36 0.4801		0.0252 4 9.9748	70° 40′
19° 30′ 19° 40′	9.5235 36 0.4765	9.5491 40 0.4509	0.0257 4 9.9743	70° 30′
	9.5270 35 0.4730		0.0261 5 9.9739	70° 20′
19° 50′	9.5306 35 0.4694	9.5571 40 0.4429	0.0266 5 9.9734	70° 10′
20° 00′	9.5341 35 0.4659	9.5611 39 0.4389	0.0270 5 9.9730	70° 00′
20° 10′	9.5375 34 0.4625	9.5650 39 0.4350	0.0275 5 9.9725	69° 50′
20° 20′	9.5409 34 0.4591	9.5689 39 0.4311	0.0279 5 9.9721	69° 40′
20° 30′	9.5443 34 0.4557	9.5727 39 0.4273	0.0284 5 9.9716	69° 30′
20° 40′ 20° 50′	9.5477 33 0.4523		0.0289 5 9.9711	69° 20′
	9.5510 33 0.4490	9.5804 38 0.4196	0.0294 5 9.9706	69° 10′
21° 00′	9.5543 33 0.4457	9.5842 38 0.4158	0.0298 5 9.9702	69° 00′
21° 10′	9.5576 33 0.4424	9.5879 38 0.4121	0.0303 5 9.9697	68° 50′
21° 20′	9.5609 32 0.4391	9.5917 37 0.4083	0.0308 5 9.9692	68° 40 ′
21° 30′ 21° 40′	9.5641 32 0.4359	9.5954 37 0.4046	0.0313 5 9.9687	68° 30′
21° 50′	9.5673 32 0.4327		0.0318 5 9.9682	68° 20′ 68° 10′
	9.5704 32 0.4296	9.6028 37 0.3972	0.0323 5 9.9677	08, 10
22° 00′	9.5736 31 0.4264	9.6064 36 0.3936	0.0328 5 9.9672	68° 00′
22° 10′	9.5767, 31 0.4233		0.0333 5 9.9667	67° 50′
22° 20′	9.5798 31 0.4202	0.0000	0.0339 5 9.9661	67° 40′
22° 30′ 22° 40′	9.5828 30 0.4172	9.6172 36 0.3828	0.0344 5 9.9656	67 30' 67° 20'
22° 50′	9.5859 30 0.4141 9.5889 30 0.4111	9.6208 36 0.3792 9.6243 35 0.3757	0.0349 5 9.9651 0.0354 5 9.9646	67° 20'
23° 00′	9.5919 30 0.4081	9.6279 35 0.3721	0.0360 5 9.9640	67° 00′
23° 10′	9.5948 30 0.4052	9,6314 35 0,3686	0.0365 5 9.9635	66° 50′
23° 20′	9.5978 29 0.4022		0.0371 5 9.9629	66° 40′
23° 30′	9.6007 29 0.3993		0.0376 5 9.9624	66° 30′
23° 40′	9,6036 29 0,3964		0.0382 6 9.9618	66° 20′
23° 50′	9.6065 29 0.3935		0.0387 6 9.9613	66° 10′
24° 00′	9.6093 28 0.3907	9.6486 34 0.3514	0.0393 6 9.9607	66° 00′
	lcosθ lsecθ	letn θ ltan θ	l cac 0 l sin 0	θ

φ	lsinφ lcscφ	ltanφ lctnφ	l sec φ l cos φ	
24° 00′	9.6093 28 0.3907	9.6486 34 0,3514	0.0393 6 9.9607	66° 00′
24° 10′	9.6121. 28 0.3879	9.6520 34 0.3480	0.0398 6 9.9602	65° 50′
24° 20′	9.6149 28 0.3851		0.0404 6 9.9596	65° 40′
24° 30′	9.6177 28 0.3823		0.0410 6 9.9590	65° 30′
24° 40′	9.6205 28 0.3795		0.0416 6 9.9584	65° 20′
24° 50′	9.6232 27 0.3768	9.6654 33 0,3346	0.0421 6 9.9579	65° 10′
25° 00'	9.8259 27 0.3741	9.6687 33 0.3313	0.0427 6 9.9573	65° 00′
25° 10′	9.6286 27 0.3714	9.6720 33 0.3280	0.0433 6 9.9567	64° 50′
25° 20′	9.6313 27 0.3687	9.6752 33 0.3248	0.0439 6 9.9561	64° 40′
25° 30′	9.6340 26 0.3660	4.0.00 00 0.0220	0.0445 6 9.9555	64° 30′
25° 40′	9.6366 26 0.3634	1 0.000	0.0451 6 9.9549	64° 20′
25° 50′	9.6392 26 0.3608	9.6850 32 0.3150	0.0457 6 9.9543	64° 10′
26° 00′	9.6418 26 0.3582	9.6882 32 0.3118	0.0463 6 9.9537	64° 00′
26° 10′	9.6444 26 0.3556		0.0470 6 9.9530	63° 50′
26° 20′	9.6470 26 0.3530		0.0476 6 9.9524	63° 40′
26° 30′	9.6495 25 0.3505	0.000.000000	0.0482 6 9.9518	63° 30′
26° 40′	9.6521 25 0.3479		0.0488 6 9.9512	63° 20′
26° 50′	9.6546 25 0.3454	9,7040 31 0.2960	0.0495 6 9,9505	63° 10′
27° 00′	9.6570 25 0.3430	9.7072 31 0.2928	0.0501 6 9.9499	63° 00′
27° 10′	9.6595 25 0.3405		0.0508 6 9.9492	62° 50′
27° 20′	9.6620 24 0.3380		0.0514 7 9.9486	62° 40′
27° 30′	9.6644 24 0.3356	1	0.0521 7 9.9479	62° 30′
27° 40′ 27° 50′	9.6668 24 0.3332	***************************************	0.0527 7 9.9473	62° 20′
	9.6692 24 0.3308	9.7226 31 0.2774	0.0534 7 9.9466	62° 10′
28° 00′	9.6716 24 0.3284	9.7257 30 0.2743	0.0541 7 9.9459	62° 00′
28° 10′	9.6740 24 0.3260		0.0547 7 9.9453	61° 50′
28° 20′	9.6763 23 0.3237	011021 00 012000	0.0554 7 9.9446	61° 40′
28° 30′	9.6787 23 0.3213		0.0561 7 9.9439	61° 30′
28° 40′	9.6810 23 0.3190	1 0.1 0.0 00 0.2022	0.0568 7 9.9432	61° 20′
28° 50′	9.6833 23 0.3167	9.7408 30 0.2592	0.0575 7 9.9425	61° 10′
29° 00′	9.6856 23 0.3144	9.7438 30 0.2562	0.0582 7 9.9418	61° 00′
29° 10′	9.6878 23 0.3122	011 101 00 012000	0.0589 7 9.9411	60° 50′
29° 20′	9.6901 22 0.3099	011 201 00 012000	0.0596 7 9.9404	60° 40′
29° 30′	9.6923 22 0.3077	9.7526 29 0.2474	0.0603 7 9.9397	6 0 ° 30′
29° 40′	9.6946 22 0.3054	0.1000 20 0.2111	0.0610 7 9.9390	60° 20′
29° 50′	9,6968 22 0,3032	9.7585 29 0.2415	0,0617 7 9.9383	60° 10′
30° 00′	9.6990 22 0.3010	9.7614 29 0.2386	0.0625 7 9.9375	60° 00′
30° 10′	9.7012 22 0.2988		0.0632 7 9.9368	59° 50′
30° 20′	9.7033 22 0.2967	9.7673 29 0.2327	0.0639 7 9.9361	59° 40′
30° 30′	9.7055 21 0.2945	9.7701 29 0.2299	0.0647 7 9.9353	59° 30′
30° 40′	9.7076 21 0.2924		0.0654 7 9.9346	59° 20′
30° 50′	9.7097 21 0.2903	9.7759 29 0.2241	0.0662 8 9.9338	59° 10′
31° 00′	9.7118 21 0 .2882	9.7788 29 0.2212	0.0669 8 9.9331	59° 00′ (
	lcos 0 l sec 0	letn 0 I tan 0	lcsc 0 lsin	0 0

φ	lsinφ lese φ	ltanφ lctnφ	lsecφ lcosφ	
31° 00′	9.7118 21 0.2882	9.7788 29 0.2212	0.0669 8 9.9331	59° 00′
31° 10′ 31° 20′	9.7139 21 0.2861 9.7160 21 0.2840	9.7816 29 0.2184 9.7845 28 0.2155	0.0677 8 9.9325 0.0685 8 9.9315	58° 50′ 58° 40′
31° 30′	9.7181 21 0.2819	9.7873 28 0.2127	0.0692 8 9.9308	58° 30'
31° 40′	9.7201 20 0.2799	9.7902 28 0.2098	0.0700 8 9.9300	58° 20′
31° 50′	9.7222 20 0.2778	9.7930 28 0.2070	0.0708 8 9.9292	58° 10′
32° 00′	9.7242 20 0.2758	9.7958 28 0.2042	0.0716 8 9.9284	58° 00′
32° 10′	9.7262 20 0.2738	9.7986 28 0.2014	0.0724 8 9.9276	57° 50′
32° 20′	9.7282 20 0.2718	9.8014 28 0.1986	0.0732 8 9.9268	57° 40′
32° 30′	9.7302 20 0.2698	9.8042 28 0.1958	0.0740 8 9.9260	57° 30′
32° 40′	9.7322 20 0.2678	9.8070 28 0.1930	0.0748 8 9.9252	57° 20′
32° 50′	9.7342 20 0.2658	9.8097 28 0.1903	0.0758 8 9.9244	57° 10′
33° 00′	9.7361 19 0.2639	9.8125 28 0.1875	0.0764 8 9.9236	57° 00′
33, 10,	9.7380 19 0.2620	9.8153 28 0.1847	0.0772 8 9.9228	56° 5 0 ′
33° 20′	9.7400 19 0.2600 9.7419 19 0.2581	9.8180 28 0.1820	0.0781 8 9.9219	56° 40′
33° 30′ 33° 40′	9.7438 19 0.2562	9.8208 27 0.1792 9.8235 27 0.1765	0.0789 8 9.9211 0.0797 8 9.9203	56° 30′ 56° 20′
33° 50′	9.7457 19 0.2543	9.8263 27 0.1737	0.0797 8 8.9203	56° 20'
34° 00′	9.7476 19 0.2524	9.8290 27 0.1710	0.0814 9 9.9186	56° 00′
34° 10′				55° 50′
34° 20′	9.7494 19 0.2506 9.7513 18 0.2487	9.8317 27 0.1683 9.8344 27 0.1656	0.0823 9 9.9177 0.0831 9 9.9169	55° 40′
34° 30′	9.7531 18 0.2469	9.8371 27 0.1629	0.0840 9 9.9160	55° 30′
34° 40′	9.7550 18 0.2450	9.8398 27 0.1602	0.0849 9 9.9151	55° 20′
34° 50′	9.7568 18 0.2432	9.8425 27 0.1675	0.0858 9 9.9142	55° 10′
35° 00′	9.7586 18 0.2414	9.8452 27 0.1548	0.0866 9 9.9134	55° 00′
35° 10′	9.7604 18 0.2396	9.8479 27 0.1521	0.0875 9 9.9125	54° 50′
35° 20′	9.7622 18 0.2378	9.8506 27 0.1494	0.0884 9 9.9116	54° 40′
35° 30′	9.76 4 0 18 0.2360	9.8533 27 0.1467	0.0893 9 9.9107	54° 30′
35° 40′	9.7657 18 0.2343	9.8559 27 0.1441	0.0902 9 9.9098	54° 20′
35° 50′	9.7675 17 0.2325	9.8586 27 0.1414	0.0911 9 9.9089	54° 10′
36° 00′	9.7692 17 0.2308	9.8613 27 0.1387	0.0920 9 9.9080	54° 00 ′
36° 10′	9.7710 17 0.2290	9.8639 27 0.1361	0.0930 9 9.9070	53° 50′
36° 20′	9.7727 17 0.2273	9.8666 26 0.1334	0.0939 9 9.9061	53° 40′
36° 30′	9.7744 17 0.2256	9.8692 26 0.1308	0.0948 9 9.9052	53° 30′
36° 40′ 36° 50′	9.7761 17 0.2239 9.7778 17 0.2222	9.8718 26 0.1282 9.8745 26 0.1255	0.0958 9 9.9042 0.0967 9 9.9033	53° 20′ 53° 10′
37° 00′	9.7795 17 0.2205	9.8771 26 0.1229	0.0977 10 9.9023	53° 00′
37° 10′	9.7811 17 0.2189	9.8797 26 0.1203	0.0986 10 9.9014	52° 50′
37° 20′	9,7828 17 0.2172	9.8824 26 0.1176	0.0996 10 9.9004	52° 40′
37° 30′	9.7844 16 0.2156	9.8850 26 0.1150	0.1005 10 9.8995	52° 30′
37° 40′ 37° 50′	9.7861 16 0.2139 9.7877 16 0.2123	9.8876 26 0.1124 9.8902 26 0.1098	0.1015 10 9.8985 0.1025 10 9.8975	52° 20′ 52° 10′
38° 00′	9.7893 16 0.2107	9.8928 26 0.1072	0.1035 10 9.8965	52° 00′
	lcosθ lsecθ	letn θ ltan θ	lcsc 0 lsin 0	0

φ	¹sinφ lese φ	ltanφ letnφ	l sec φ l cos φ	
38° 00′	9.7893 16 0.2107	9.8928 26 0.1072	0.1035 10 9.8965	52° 00′
				1 1
38° 10′	9.7910 16 0.2090	9.8954 26 0.1046	0.1045 10 9.8955	51° 50′
38° 20′	9.7926 16 0.2074	9.8980 26 0.1020	0.1055 10 9.8945	51° 40′
38° 30′ 38° 40′	9.7941 16 0.2059	9.9006 26 0.0994	0.1065 10 9.8935	51° 30′
38° 50′	9.7957 16 0.2043 9.7973 16 0.2027	9.9032 26 0.0968 9.9058 26 0.0942	0.1075 10 9.8925	51° 20′ 51° 10′
	8.7973 16 0.2027	9,8008 26 0,0842	0.1085 10 9.8915	01, 10
39° 00′	9.7989 16 0.2011	9.9084 26 0.0916	0.1095 10 9.8905	51° 00′
39° 10′	9.8004 16 0.1996	9.9110 26 0.0890	0.1105 10 9.8895	50° 50′
39° 20′	9.8020 15 0.1980	9.9135 26 0.0865	0.1116 10 9.8884	50° 40′
39° 30′	9.8035 15 0.1965	9.9161 26 0.0839	0.1126 10 9.8874	50° 30′
39° 40′	9.8050 15 0.1950	9.9187 26 0.0813	0.1136 10 9.8864	50° 20′
39° 50′	9.8066 15 0.1934	9.9212 26 0.0788	0.1147 11 9.8853	50° 10′
40° 00′	9.8081 15 0.1919	9.9238 26 0.0762	0.1157 11 9.8843	50° 00′
40° 10′	9.8096 15 0.1904	9.9264 26 0.0736	0.1168 11 9.8832	49° 50′
40° 20′	9.8111 15 0.1889	9.9289 26 0.0711	0.1179 11 9.8821	49° 40′
40° 30′	9.8125 15 0.1875	9.9315 26 0.0685	0.1190 11 9.8810	49° 30′
40° 40′	9.8140 15 0.1860	9.9341 26 0.0659	0.1200 11 9.8800	49° 20′
40° 50′	9.8155 15 0.184 5	9.9366 26 0.0634	0.1211 11 9.8789	49° 10′
41° 00′	9.8169 15 0.1831	9.9392 26 0.0608	0.1222 11 9.8778	49° 00′
41° 10′	9.8184 14 0.1816	9.9417 25 0.0583	0.1233 11 9.8767	48° 50′
41° 20′	9.8198 14 0.1802	9.9443 25 0.0557	0.1244 11 9.8756	48° 40′
41° 30′	9.8213 14 0.1787	9.9468 25 0.0532	0.1255 11 9.8745	48° 30′
41° 40′	9.8227 14 0.1773	9.9494 25 0.0506	0.1267 11 9.8733	48° 20′
41° 50′	9.8241 14 0.1759	9.9519 25 0.0481	0.1278 11 9.8722	48° 10′
42° 00′	9.8255 14 0.1745	9.9544 25 0.0456	0.1289 11 9.8711	48° 00′
42° 10′	9.8269 14 0.1731	9.9570 25 0.0430	0.1301 11 9.8699	47° 50′
42° 20′	9.8283 14 0.1717	9.9595 25 0.0405	0.1312 12 9.8688	47° 40′
42° 30′	9.8297 14 0.1703	9.9621 25 0.0379	0.1324 12 9.8676	47° 30′
42° 40′	9.8311 14 0.1689	9.9646 25 0.0354	0.1335 12 9.8665	47° 20′
42° 50′	9.8324 14 0.1676	9.9671 25 0.0329	0.1347 12 9.8653	47° 10′
43° 00′	9.8338 14 0.1662	9.9697 25 0.0303	0.1359 12 9.8641	47° 00′
43° 10′	9,8351 13 0,1649	9.9722 25 0.0278	0,1371 12 9,8629	46° 50′
43° 20′	9.8365 13 0.1635	9.9747 25 0.0278	0.1382 12 9.8618	46° 40′
43° 30′	9.8378 13 0.1622	9.9772 25 0.0238	0.1394 12 9.8606	46° 30′
43° 40′	9.8391 13 0.1609	9.9798 25 0.0202	0.1406 12 9.8594	46° 20′
43° 50′	9.8405 13 0.1595	9.9823 25 0.0177	0.1418 12 9.8582	46° 10′
44° 00′	9.8418 13 0.1582	9.9848 25 0.0152	0.1431 12 9.8569	46 ° 00′
44° 10′	9.8431 13 0.1569	9.9874 25 0.0126	0.1443 12 9.8557	45° 50′
44° 20′	9.8444 13 0.1556	9.9899 25 0.0101	0.1455 12 9.8545	45° 40′
44° 30′	9.8457 13 0.1543	9.9924 25 0.0076	0.1468 12 9.8532	45° 30′
44° 40′	9.8469 13 0.1531	9.9949 25 0.0051	0.1480 12 9.8520	45° 20′
44° 50′	9.8482 13 0.1518	9.9975 25 0.0025	0.1493 13 9.8507	45° 10′
45° 00′	9.8495 13 0.1505	0.0000 25 0.0000	0.1505 13 9.8495	 45° 00 ′
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Inverse Circular Functions.

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42						38.46 64 51.54
43						39.11 65 50.89
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45 16.37 39 73.63 15.74 34 74.26 95 63.03 26.97 41.71 66 48.29 46 16.76 40 73.24 16.09 35 73.91 96 65.78 24.22 42.37 66 47.63 47 17.16 41 72.84 16.44 36 73.56 97 68.95 21.05 43.02 66 46.98 48 17.58 42 72.42 16.80 37 73.20 98 72.74 17.26 43.68 66 46.32			l v			40.40 65 49.60
46	44	15.99 38 74.01	15.40 34 74.60	94	60.57 29.43	41.05 65 48.95
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49 10 00 40 70 00 17 17 07 70 00 00 17 17 17 10 00 14 04 00 45 22	/ 48 }					43.68 66 46.32
1 TOLOG 43 12 OU TITL 31 12 OO 88 11/10 TS/50 44/24 66 40.00	49 .	18.00 43 72.00	17.17 37 72.83	99	77.75 12.25	44.34 66 45.66
18.43 44 71.57 17.55 38 72.45 00 90.00 00.00 45.00 66 45.0	50 TT	8.43 44 71 57	17.55 20 79.45	100	90.00 00.00	45.00 66 45.00

Inverse Circular Functions.

log u	sin-l u		cos-1 u	log u	sin-1 u		cos-1 u	log u	sin-1 u		cos-l u
9.	9		۰	9.	0		0	9.	0		0
750	34.22	9	55.78	800	39.12	11	50.88	850		13	44.93
751	34.31	9	55.69	801	39.23	11	50.77	851		13	44.80
752	34.40	9	55.60	802	39.34	11	50.66	852		13	44.67
753	34.49	9	55.51	803	39.44	11	50.56	853		13	44.53
75 4	34.58	9	55.42	804	39.55	11	5 0.4 5	854	45.60	13	44.40
755	34.67	9	55.33	805	39.66	11	50.34	855	45.74	14	44.26
756	34.76	9	55.24	806	39.77	11	50.23	856	45.87	14	44.13
767	34.85	9	56.15	807	39.88	11	50.12	857	46.01	14	43.99
758	34.95	9	55.05	808	39.99	11	50.01	858	46.1 5	14	43.85
759	35.04	9	54.96	809	40.10	11	49.90	859	46.28	14	43.72
760	35.13	9	54.87	810	40.21	11	49.79	860	46.42	14	43.58
761	35.22	9	54.78	811	40.33	11	49.67	861			43.44
762	35.32	9	54.68	812	40.44	11	49.56	862			43.30
763	35.41	9	54.59	813	40.55	11	49.45	863			43.16
764	35.50	9	54.50	814	40.66	11	49.34	864			43.02
765	35,60	9	54.40	815	40.78	11	49.22	865	47.12	_	42.88
766	35.69	9	54.31	816	40.89	11	49.11	866			42.73
767	35.79	10	54.21	817	41.01	11	48.99	867			42.59
768	35.88	10	54.12	818	41.12	12	48.88	868			42.45
769	35.98	10	54.02	819	41.24	12	48.76	869			42.30
770	36.07	10	53.93	820	41.35	12	48.65	870		-	42.16
771 772	36.17 36.27	10	53.83	821 822	41.47 41.59	12	48.53	871 872			42.01 41.86
773	36.36	10 10	53.73 53.64	822 823	41.70	12 12	48.41 48.30	872 873			41.72
774	36.46	10	53.54	823 824	41.70	12	48.18	874			41.72
						_					
775	36.56	10	53.44	825	41.94	12	48.06	875			41.42
776	36.66	10	53.34	826	42.06	12	47.94	876 877			41.27
777	36.76	10	53.24	827	42.18	12	47.82	877			41.12
778 779	36.85	10	53.15	828	42.3 0 42.4 2	12	47.70 47.58	878 879			40.97 40.81
	36.95	10	53.05	829	_	12					
780	37.05	10	52.95	830	42.54	12	47.46	880			40.66
781	37.15	10	52.85	831	42.66	12	47.34	881			40.51
782	37.25	10	52.75	832	42.78	12	47.22	882			40.35
783	37.35	10	52.65	833	42.90	12	47.10	883			40.20
784	37.45	10	5 2.5 5	834	43.03	12	46.97	884		_	40.04
785	37.56	10	52.44	835	43.15	12	46.85	885			39.88
786	37.66	10	52.34	836	43.27	12	46.73	886		16	39.72
787	37.76	10	52.24	837	43.40	12	46.60	887			39.56
788	37.86	10	52.14	838	43.52	13	46.48	888			39.40
789	37.96	10	52.04	839	43.65	13	46.35	889	50.7 6	16	39.24
790	38.07	10	51.93	840	43.78	13	46.22	890			39.08
791	38.17	10	51.83	841	43.90	13	46.10	891			38.92
792	38.28	10	51.72	842	44.0 3	13	45.97	892			38.75
793	38.38	10	51.62	843	44.16	13	45.84	893	-	17	38.59
794	38.4 8	10	51.52	844	44.2 9	13	45.71	894	51.58	17	38.42
795	38.59	11	51.41	845	44.41	13	45.59	895	51.74	17	38.26
796	38.69	11	51.31	846	44.54	13	45.46	896	51.91	17	38.09
797	38.80	11	51.20	847	44.67	13	4 5. 3 3	897		17	37.92
798	38.91	11	51.09	848	44.8 0	13	45.20	888		77	31.12
799	39.01	11	50.99	849	44.94	13	45.0 €	888	68.42	1	
800 l	39.12	11	50.88	850	45.07	1	3 44.9	0 e E	0 \ 58.E	· 10	12 21

Inverse Circular Functions.

$\log u$	sin-1 <i>u</i> cos-1 <i>u</i>	log u	sin-1 u cos-1 u	log u	sin-1 u	log u	sin-1 u
9.	0 0	9.	0 0	9.	۰	9.	۰
900	52.59 17 37.41	950	63.03 26 26.97	9900	77.75	9950	81.32
901	52.76 17 37.24	951	63.29 26 26.71	9901	77.81	9951	81.41
902	52.94 17 37.06	952	63.56 27 26.44	9902	77.87	9952	81.50
903	53.11 18 (6.89	953	63.82 27 26.18	9903	77.94	9953	81.59
904	5 3.29 1 8 36.71	954	64.09 27 25.91	9904	78. 0 0	9954	81.68
905	53.47 18 36.53	955	64.37 27 25.63	9905	78.06	9955	81.77
906	53.65 18 36.35	956	64.64 28 25.36	9906	78.12	9956	81.86
907	53.83 18 36.17	957	64.92 28 25.08	9907	78.18	9957	81.95
908	54.01 18 35.99	958	65.21 20 24.79	9908	78.25	9958	82.04
909	54.19 18 35.81	950	65.40 29 24.51	9909	78.31	9959	82.14
910	54.37 18 35.6 3	960	65.78 29 24.22	9910	78.38	9960	82.24
911	54.56 19 35.44	961	66.08 30 23.92	9911	78.44	9961	82.33
912	54.74 19 35.2 6	962	66.38 30 23.62	9912	78.50	9962	82.43
913	54.93 19 35.07	963	66.68 31 23.32	9913	78.57	9963	82.5
914	55.12 19 34.88	964	66.99 31 23.01	9914	78.64	9964	82.6
915	55.31 19 34.69	965	67.30 32 22.70	9915	78,70	9965	82.7
916	55.50 19 34.50	966	67.62 32 22.38	9916	78.77	9966	82.8
917	55.69 19 34.31	967	67.95 33 22.05	9917	78.83	9967	82.9
918	55.89 19 34.11	968	68.27 33 21.73	9918	78.90	9968	83.1
919	56.08 20 33.92	969	68.61 34 21.39	9919	78.97	9969	83.2
i l		ľ					
920	56.28 20 33.72	970	68.95 34 21.05	9920	79.04	9970	83.3
921	56.48 20 33.52	971	69.29 35 20.71	9921	79.10	9971	83.4
922	56.68 20 33.32	972	69.65 36 20.35	9922	79.17	9972	83.5
923	56.88 20 33.12	978	70.01 36 19.99	9923	79.24	9973	88. c
924	57.08 20 32.92	974	70.37 37 19.63	9924	79.31	9974	83.7
925	57.29 21 32.71	975	70.75 38 19.25	9925	79.38	9975	83.9
926	57.49 21 32.51	976	71.13 39 18.87	9926	79.45	9976	84.0
927	57.70 21 32.30	977	71.52 39 18.48	9927	79.52	9977	84.1
928	57.91 21 32.09	978	71.92 40 18.08	9928	79.60	9978	84.2
929	58.12 21 31.88	979	72.83 41 17.67	9929	79.67	9979	84.4
1) 1						0080	
930	58.34 21 31.66	980	72.74 42 17.26	9930	79.74	9980	84.5
931	58.55 22 31.45	981	73.18 44 16.82	9931	79.81	9981	84.6
932	58.77 22 31.23	982	73.63 45 16.38	9932	79.89	9982 9983	84.8
933	58.99 22 31.01	983	74.0, 46 15.93	9933	79.96		84.9
934	59.21 22 30.79	984	74.5 4 48 15.46	9934	80.04	9984	85.1
935	59.43 22 30.57	985	75.03 49 14.97	9935	80.11	9985	85.2
936	59.65 23 30.35	986	75.53 51 14.47	9936	80.19	9986	85.4
937	59.88 23 30.12	987	76.05 53 13.95	9937	80.26	9987	85.6
938	60.11 23 29.89	988	/6.59 55 13.41	9938	80.34	9988	85.7
939	60.34 23 29.66	989	77.16 58 12.84	9939	80.42	9989	85.9
940	60.57 23 29.43	990	77.75 61 12.25	9940	80.50	9990	86.1
941	60.81 24 29.19	991	78.38 11 62	9941	80.58	9991	86.3
942	61.04 24 28.96	992	79.04 10.96	9942	80.66	9992	86.5
943	61.28 24 28.72	993	79.74 10.26	9943	80.74	9993	86.7
944	61.52 24 28.48	994	80.50 9.50	9944	80.82	9994	87.0
945	61.77 25 28.23	995	81.32 8.68	9945	80.90	9995	87.3
946	62.02 25 27.98	996	82.24 7.76	9946	80.98	9996	87.5
947	62.27 25 27.73	997	83.3 6.7	9947	81.07	9997	87.9
948	62.52 25 27.48	998	84.3 6.8	9948	81.15	9998	88.3
949	62.7 7 26 27.23	999	86.1 3.9	9949	81.24	8888	888
950 F	3.03 26 26.97	000	90, 0,	70050	1 87 30	2000 [3	80.

Logarithms of Hyperbolic Functions.

								1
x	$\operatorname{\mathbf{gd}} x$	x	$\operatorname{\mathbf{gd}} x$	x	$1 \operatorname{Sh} x$	l Ch x	l Th x	
	0		°		0.	0.	9.	
0.00	0.0000 5730	0.50	27.524 508	1.00	0701 57	1884 33	8817 24	Ł
0.01	0.5729 5729	0.51	28.031 506	1.01	0758 57	1917 33	8840 23	ł
0.02	1.1458 5728	0.52	28.535 503	1.02	0815 56	1950 33	8864 23	ı
0.03	1.7186 5727	0.58	29.037 501 29.537 498	1.03	0871 56 0927 56	1984 34	8887 23	ı
0.04	2.2912 5725	0.54		1.04		2018 34	8909 22	1
0.05	2.8636 5722	0.55	30.034 496	1.05	0982 56	2051 34	8931 22	ı
0.06	3.4357 5719	0.56	30.529 494	1.06	1038 55	2086 34	8952 21	
0.07	4.0074 5716	0.57	31.021 491	1.07	1093 55	2120 34	8978 21	
0.08	4.5788 5711	0.58	31.511 488	1.08	1148 55	2154 31	8994 20	ł
0.09	5.1497 5706	0.59	31,998 486	1.09	1203 54	2189 35	9014 20	l
.10	5.720 570	0.60	32.483 483	1.10	1257 54	2223 35	9034 19	1
0.11	6.290 570	0.61	32.965 481	1.11	1311 54	2258 33	9053 19	ı
0.12	6.859 569	0.62	33.444 478	1.12	1365 51	2293 35	9072 10	ı
0.13 0.14	7.428 568	0.63	33.921 475	1.13	1419 54	2328 35	9090 18	ı
l i	7.995 567	0.64	34.395 473	1.14	1472 53	2364 35	9108 13	ı
0.15	8.562 567	0.65	34.867 470	1.15	1525 53	2399 26	9126 18	I
0.16	9.128 566	0.66	35.336 467	1.16	1578 53	2435 36	9144 17	1
0.17	9.694 565	0.67	35.802 465	1.17	1631 53	2470 36	9161 17	l
0.18 0.19	10.258 564	0.68	36.265 462	1.18 1.19	1684 52	2506 36	9177 17	ł
1 .	10.821 563	0.69	36.726 459		1736 52	2542 36	9194 16	ı
0.20	11.384 562	0.70	37.183 456	1.20	1788 52	2578 36	9210 16	ı
0.21	11.945 561	0.71	37.638 454	1.21	1840 52	2615 36	9226 16	ı
0.22	12.505 559	0.72	38.091 451	1.22	1892 52	2651 36	9241 15	ı
0.23	13.063 558	0.73	38.5 4 0 448	1.23	1944 52	2688 37	9256 15	ı
0.24	13.621 557	0.74	38.987 445	1.24	1995 51	2724 37	9271 15	1.
0.25	14.177 556	0.75	39.431 443	1.25	204 6 51	2761 37	9285 14	Γ
0.26	14.782 554	0.76	39.872 440	1.26	2098 51	2798 37	9300 14	l
0.27	15.285 553	0.77	40.310 437	1.27	2148 51	2885 37	9314 14	l
0.28	15.837 551	0.78	40.746 434	1.28	2199 51	2872 37	9327 14	ľ
0.29	16.388 550	0.79	41.179 431	1.29	2250 51	2909 37	9341 13	ľ
0.30	16.937 548	0.80	41.608 428	1.30	2300 50	2947 37	9354 13	l
0.51	17.484 546	0.81	42.035 426	1.31	2351 50	2984 38	9367 13	1
0.32	18.030 545	0.82	42.460 423	1.32	2401 50	3022 38	9379 12	1
0.33	18.573 543	0.88	42.881 420	1.33	2451 50	3059 38	9391 12	1
0.34	19.116 541	0.84	43.299 417	1.34	2501 50	3097 38	9404 12	1
0.35	19.656 540	0.85	43.715 414	1.35	2551 50	3135 38	9415 12	1
0.86	20.195 538	0.86	44.128 411	1.36	2600 50	3173 38	9427 11	1
0.37	20.732 536	0.87	44.537 408	1.37	2650 49	3211 38	9438 11	
0.38	21.267 534	0.88	44.944 406	1.38	2699 49	3249 38	9450 11	
0.39	21.800 532	0.89	45.348 403	1.39	2748 49	3288 38	9460 11	
0.40	22.331 530	0.90	45.750 400	1.40	2797 49	3326 38	9471 11	1
0.41	22.859 528	0.91	46.148 397	1.41	2846 49	3365 39	9482 10	1
0.42	23.386 526	0.92	46.544 394	1.42	2895 49	3403 39	9492 10	1
0.43	23.911 524	0.93	46.936 391	1.48	2944 49	3442 39	9502 10	ı
0.44	24.434 522	0.94	47.326 388	1.44	2993 49	3481 39	9512 10	1
0.45	24.955 519	0.95	47.713 386	1.45	3041 48	3520 39	9522 10	1
0.46	25.473 517	0.96	48.097 383	1.46	3090 48	3559 39	9531 9	ı
0.47	25.989 515	0.97	48.478 380	1.47	3138 48	3598 39	9540 9	l
0.48	26.503 513	0.98	48.857 377	1.48	3186 48	8837 39	8540 0	1.
0,49	27.015 510	0.99	49.232 374	1.49	3834 4			8
0.50	27.524 508	1.00	49.605 371	71.50	0 3282	48 / 377 E	39 / 828.	<u>`</u>

Logarithms of Hyperbolic Functions.

x	l Sh x	l Ch x	l Th x	x	1 Sh x	l Ch x	l Th x
	0.	0.	9.		0.	0.	9.
1.50	3282 48	3715 39	9567 9	2.00	5595 45	575 4 42	9841 3
1.51	3330 48	3754 39	9576 8	2.01	5640 45	5796 42	9844 3
1.52	3378 48	3794 39	9584 8	2.02	5685 45	5838 42	9847 3
1,53	3426 48	3833 40	9592 8	2.03	5730 45	5880 42	9850 з
1.54	3474 48	3873 40	9601 8	2.04	5775 45	5922 42	9853 3
1.55	3521 48	3913 40	9608 8	2.05	5820 45	5964 42	9856 3
1.56	3569 47	3952 40	9616 8	2.06	5865 45	6006 42	9859 3
1.57	3616 47	3992 40	9624 8	2.07	5910 45	6048 42	9862 3
1.58	3663 47	4032 40	9631 7	2.08	5955 45	6090 42	9864 3
1.59	3711 47	4072 40	9639 7	2.09	6000 45	6132 42	9867 3
1.60	3758 47	4112 40	9646 7	2.10	6044 45	6175 42	9870 з
1.61	3805 47	4152 40	9653 7	2.11	6089 45	6217 42	9872 3
1.62	3852 47	4192 40	9660 7	2.12	6134 45	6259 42	9875 3
1.63	3899 47	4232 40	9666 7	2.13	6178 45	6301 42	9877 2
1.64	3946 47	4273 40	9673 7	2.14	6223 45	6343 42	9880 2
1							
1.65	3992 47	4313 40	9679 6	2.15	6268 45	6386 42	9882 2
1.66	4039 47	4353 40	9686 6	2.16	6312 45	6428 42	9884 2
1.67	4086 47	4394 40	9692 6	2.17	6357 45	6470 42	9887 2
1.68	4132 47	4434 41	9698 6	2.18	6401 45	6512 42	9889 2
1.69	4 179 46	4475 41	9704 6	2.19	6446 45	6555 42	9891 2
1.70	4225 46	4515 41	9710 6	2.20	6491 45	6597 42	9893 2
1.71	4272 46	4 556 41	9716 6	2.21	6535 44	6640 42	9895 2
1.72	4318 46	4597 41	9721 6	2.22	6580 44	6682 42	9898 2
1.73	4364 46	4637 41	9727 5	2.23	6624 44	6724 42	9900 2
1.74	4411 46	4678 41	9732 5	2.24	6668 44	6767 42	9902 2
1.75	4457 46	4719 41	9738 5	2.25	6713 44	6809 42	9904 2
1.76	4503 46	4760 41	9743 5	2.26	6757 44	6852 42	9905 2
1.77	4549 46	4801 41	9748 5	2.27	6802 44	6894 43	9907 2
1.78	4595 46	4842 41	9753 B	2.28	6846 44	6937 43	9909 2
1.79	4641 46	4883 41	9758 5	2.29	6890 44	6979 43	9911 2
1.80	4687 46	4924 41	9763 5	2.30	6935 44	7022 43	9913 2
1.81	4733 46	4965 41	9767 B	2.31	6979 44	7064 43	9914 2
1.82	4 778 46	5006 41	9772 5	2.32	7023 44	7107 43	9916 2
1.83	4824 46	5048 41	9776 4	2.33	7067 44	7150 43	9918 2
1.84	4870 46	5089 41	9781 4	2.34	7112 44	7192 43	9919 2
1.85	4915 46 4961 46	5130 41 5172 41	9785 4 9789 4	2.35	7156 44 7200 44	1	9921 2 9923 2
1.86				2.36			
1.87	5007 46	5213 41	9794 4	2.37	7244 44	7320 43	9924 2
1.88	5052 46	5254 41	9798 4	2.38	7289 44	7863 43	9926 1
1.89	5098 45	5296 41	9802 4	2.39	7333 44	7406 43	9927 1
1.90	5143 45	5337 42	9806 4	2.40	7377 44	7448 43	9929 1
1.91	5188 45	5379 42	9810 4	2.41	7 4 21 44	7491 43	9930 1
1.92	5234 45	5 421 42	9813 4	2.42	7465 44	753 4 43	9931 1
1.93	5279 45	5 462 42	9817 4	2,43	7509 44	7577 43	9933 1
1.94	5324 45	5504 42	9821 4	2.44	7553 44	7619 43	9934 1
1.95	5370 45					7662 43	9935 1
1.96	5415 45		9824 4	2.45	7597 44	7002 43	9937 1
1.97	5460 45	5687 42	9828 3	2.46	7642 44		9938 1
1.98		5629 42	9831 3	2.47	7686 44	7748 43	9939 1
1.98	5505 45	5671 42	9834 3	2.48	7730 44	7791 43	
<i>F</i>	<i>5550 45</i>	<i>5713</i> 42	9838 3	2.49	7774 44	7833 43	9940 1
2.00	5595 45	5754 42	9841 3	12.50	7818 44	. \ 7876 43	s / 99 <u>4</u> 1 1

Logarithms of Hyperbolic Functions.

x	l Sh x	l Ch x	l Th x	x ,	l Sh x	l Ch x	l Th x
	0.	0.	9.				
2.50	7818 44	7876 43	9941	3.0	1.0008 436	1.0029 432	9.9978
2.51	7862 44	7919 43	9943	3.1	1.0444 436	1.0462 433	9.9982
2.52	7906 44	7962 43	9944	3.2	1.0880 436	1.0894 433	
2.53	7950 44	8005 43	9945	3.3	1.1316 435		9.9986
2.54	7994 44	8048 43	9946			1.1327 433	9.9988
				3.4	1.1751 435	1.1761 433	9.9990
2.55	8038 44	8091 43	9947	3.5	1.2186 435	1.2194 434	9.9992
2.56	8082 44	8134 43	9948	3.6	1.2621 435	1.2628 434	9.9994
2.57	8126 44	8176 43	9949	3.7	1.3056 435	1.3061 434	9.9995
2.58	8169 44	8219 43	9950	3.8	1.3491 435	1.3495 434	9.9996
2.59	8213 44	8262 43	9951	3.9	1.3925 435	1.3929 434	9.9996
2.60	8257 44	8305 43	9952	4.0	1 4960 407	1.4363 434	9.9997
2.61	8301 44	8348 43	9953	4.1	1.4360 435	1.4797 434	9.9998
2.62	8345 44	8391 43	9954	4.1 4.2	1.4795 435	1.5231 434	
2.63	8389 44	8434 43	9955		1.5229 434		9.9998
2.64	8433 44	8477 43	9956	4.3 4.4	1.5664 434	1.5665 434	9.9998
					1.6098 434	1.6099 434	
2.65	8477 44	8520 43	9957	4.5	1.6532 434	1.6533 434	9.9999
2.66	8521 44	8563 43	9958	4.6	1.6967 434	1.6968 434	9.9999
2.67	8564 44	8606 43	9958	4.7	1.7401 434	1.7402 434	9.9999
2.68	8608 44	8649 43	9959	4.8	1.7836 434	1.7836 434	9.9999
2.69	8652 44	8692 43	9960	4.9	1.8270 434	1.8270 434	0.0000
2.70	8696 44	8735 43	9961	5.0	1.8704 434	1.8705 434	0.0000
2.71	8740 44	8778 43	9962	5.1	1.9139 434	1.9139 434	0.0000
2.72	8784 44	8821 43	9962	5.2	1.9573 434	1.9573 434	0.0000
2.73	8827 44	8864 43	9963	5.3	2.0007 434	2.0007 434	0.0000
2.74	8871 44	8907 43	9964	5.4	2.0442 434	2.0442 434	0.0000
2.75							
	8915 44	8951 43	9965	5.5	2.0876 434	2.0876 434	0.0000
2.76	8959 44	8994 43	9965	5.6	2.1310 434	2.1310 434	0.0000
2.77	9003 44	9037 43	9966	5.7	2.1744 434	2.1745 434	0.0000
2.78	9046 44	9080 43	9967	5.8	2.2179 434	2.2179 434	0.0000
2.79	9090 44	9123 43	9967	5.9	2.2613 434	2.2613 434	0.0000
2.80	9134 44	9166 43	9968	6.0	2.3047 4343	2.3047 4343	0.0000
2.81	9178 44	9209 43	9969	7.0	2.7390 4343	2.7390 4343	0.0000
2.82	9221 44	9252 43	9969	8.0	3.1733 4343	3.1733 4343	0.0000
2.83	9265 44	9295 43	9970	9.0	3.6076 4343	3.6076 4343	0.0000
2.84	9309 44	9338 43	9970	10.0	4.0419 4343	4.0419 4343	0.0000
2.85	9353 44	9382 43	9971				
2.86	9396 44	9425 43	9972		For high	er values:	
2.87	9440 44	9468 43	9972	log S	$h x = \log Ch$	$x = x\mu - 0.30$	1030;
2.88	9484 44	9511 43	9973	Sh-1	$u = \operatorname{Ch}^{-1} u =$	$(\log u + 0.20)$	IU) μ ⁻¹ .
2.89	9527 44	9554 43	9973				
				n	$n\mu$	$n\mu^{-1}$	n
2.90	9571 44	9597 43	9974				
2.91	9615 44	9641 43	9974	1	0.434294	2.302585	1
2.92	9658 44	9684 43	9975	2	0.868589	4.605170	2
2.93	9702 44	9727 43	9975	3	1.302883	6.907755	3
2.94	9746 44	9770 43	9976	4	1.737178	9.210340	4
2.95	9789 44	9813 43	9976	5	2.171472	11.512925	5
2.96	9833 44	9856 43	9977	6	2.605767	13.815511	- 6
2.97	9877 44	9900 43	9977	7	3.040061	16.118096	1 7
2.98	9920 44	9943 43	9978	8	3.474358	18,420881	
2.99	9964 44	9986 43	9978	ŝ	3.908850	\$0.15356	θ I θ
3.00		1.0000 40	0070	•	4.342945	\	
0.VV	1.0008 44	1.0029 43	1 8818	10	1 4'24.7A	/ 40/040	<u></u>

Natural Sines and Cosines.

φ	sin φ	cos φ		φ	sin φ	сов ф		φ	sin φ	сов ф	
0°	.000000	1.0000	90°	70				15°	.2588	.9659	750
10'	.002909	1.0000	50′	30′	.1305	.9914	30′	10′	.2616	.9652	50′
20′	.005818	1.0000	40′	40′ 50′	.1334	.9911	20′	20′	.2644	.9644	40/
30′	.008727	1.0000	30′		.1363	.9907	10′	80′	.2672	.9636	30/
40′ 50′	.011635	0.9999	20′	8°	.1392	.9903	82°	40' 50'	.2700	.9628	20/
10	.014544	0.9999	10′ 89°	10' 20'	.1421	.9899	50′ 40′	16°	.2728	.9621	10′ 74°
11	.017452	0.9998		30	1478	.9890	30/		.2756	.9613	
10' 20'	.02036 .02327	0.9998 0.9997	50′ 40 ′	40′	.1507	.9886	20′	. 10/ 20/	.2784 .2812	.9605	50′ 40′
30'	.02618	0.9997	30/	50′	.1536	.9881	10′	30	.2840	.9588	30/
40′	.02908	0.9996	20'	9°	.1564	.9877	81 °	40′	.2868	.9580	20/
50′	.03199	0.9995	10′	10′	.1593	.9872	50′	50′	.2896	.9572	10/
2°	.03490	0.9994	880	20′	.1622	.9868	40′	17°	.2924	.9563	730
10′	.03781	0.9993	50′	30′	.1650	.9863	30′	10′	.2952	.9555	50′
20′	.04071	0.9992	40′	40′ 50′	.1679 .1708	.9858	20′	20′	.2979	.9546	40/
30′	.04362	0.9990	30/			.9853	10′	30′	.3007	.9537	30⁄
40' 50'	.04653 .04943	0.9989	20' 10'	10°	.1736	.9848	80°	40′ 50′	.3035 .3062	.9528	20′
30	_	0.9988	870	10′	.1765	.9843	50′			.9520	10′ 72°
11	.05234	0.9986		20′ 30′	.1794 .1822	.9838	40′ 30′	18°	.3090	.9511	
10' 20'	.05524	0.9985	50′	40′	.1851	.9827	20/	10′	.3118	.9502	50′
30	.05814 .06105	0.9983 0.9981	40' 30'	50′	.1880	.9822	10′	20′ 30′	.3145 .3173	.9492 .9483	40' 30'
40/	.06395	0.9980	20/	110	.1908	.9816	790	40'	.3201	.9474	20
50′	.06685	0.9978	10′	10′	.1937	.9811	50′	50'	.3228	.9465	10
4 °	.06976	0.9976	860	20′	.1965	.9805	40′	19°	.3256	.9455	710
10′	.07266	0.9974	50′	30′	.1994	.9799	30/	10′	.3283	.9446	50/
20/	.07556	0.9971	40'	40′	.2022	.9793	20′	20'	.3311	.9436	40
30′	.07846	0.9969	30/	50′	.2051	.9787	10′	30′	.3338	.9426	30/
40/	.08136	0.9967	20′	12°	.2079	.9781	78°	40′	.3365	.9417	20′
50′	.08426	0.9964	10′	10′	.2108	.9775	50′	50′	.3393	.9407	10′
5°	.08716	0.9962	85°	20′ 30′	.2136	.9769	40′	20°	.3420	.9397	70°
10′	.09005	0.9959	50′	40′	.2164	.9763 .9757	30′ 20′	10′	.3448	.9387	50′
20' 30'	.09295 .09585	0.9957 0.9954	40′ 30′	50'	.2221	.9750	10	20′	.3475 .3502	.9377 .9367	40′ 30′
40/	.09874	0.9951	20'	13°	.2250	.9744	770	30′ 40′	.3529	.9356	20'
50′	.10164	0.9948	10	10′	.2278	.9737	50′	50'	.3557	.9346	10
6°	.10453	0.9945	840	20′	.2306	.9730	40′	21°	.3584	.9336	69 °
10′	.1074	0.9942	50/	30′	.2334	.9724	30′	10′	.3611	.9325	50/
20'	.1103	0.9939	40'	40′	.2363	.9717	20′	20	.3638	.9315	40/
30′	.1132	0.9936	30′	50′	.2391	.9710	10′	30′	.3665	.9304	30′
40′	.1161	0.9932	20′	14°	.2419	.9703	76 °	40′	.3692	.9293	20′
50'	.1190	0.9929	10′	10′	.2447	.9696	50′	50'	.3719	.9283	10′
70	.1219	0.9925	83 °	20′	.2476	.9689	40/	22°	.3746	.9272	68°
10′	.1248	0.9922	50′	30′ 40′	.2504 .2532	.9681 .9674	30′ 20′	10′	.3773	.9261	50′
20′ 30′	.1276 .1305	0.9918 0.9914	40' 30'	50′	.2560	.9667	10′	20′ 30′	.3800 .3827	.9250 .9239	40′ 30′
J "	11000	0.0014	30' 82 °	15°	.2588	.9659	750	30	10041	10400	670
	cos θ	sin θ	θ		cos θ	sin 0	θ		cos θ	в тів	9

Natural Sines and Cosines.

φ	sin ø	cos ф	1	φ	sin φ	cos φ		φ	sin φ	cos φ	
200		<u>'</u>		30°	·		600	370	, 		
30'	.3827	.9239	30′		.5000		<u>60°</u>	30'	.6088	.7934	30/
40	.3854	.9228	20	10′	.5025	.8646	50′	40'	.6111	.7916	20'
50'		.9216	10'	20′	.5050	.8631	40′	50'	.6134	.7898	10'
			4	30′	.5075	.8616	30′		_		
23°	.3907	.9205	67°	40′ 50′	.5100 .5125	.8601 .8587	20′ 10′	38°	.6157	.7880	52°
10′	.3934	.9194	50′					10′	.6180	.7862	50′
20′	.3961	.9182	40′ 30′	31°	.5150	.8572	59°	20′ 30′	.6202	.7844	40′
30' 40'	.3987 .4014	.9171	20'	10′	.5175	.8557	50/	40'	.6225	.7826	30′
50'	.4041	.9147	10'	20′	.5200	.8542	40′	50/	.6271	.7808	20' 10'
				30′	.5225	.8526	30′			-	
24°	.4067	.9135	66°	40′	.5250	.8511	20′	39°	.6293	.7771	51 °
10′	.4094	.9124	50′	50′	.5275	.8496	10′	10′	.6316	.7753	50'
20'	.4120	.9112	40′	32°	.5299	.8480	58°	20'	.6338	.7735	40'
30′	.4147	.9100	30′	10′	.5324	.8465	50′	30′	.6361	7716،	30/
40'	.4173	.9088	20'	20	.5348	.8450	40'	40′	.6383	.7698	20/
50′	.4200	.9075	10′	30'	.5373	.8434	30/	50′	.6406	.7679	10′
25°	.4226	.9063	65°	40′	.5398	.8418	20′	40 °	.6428	.7660	50 °
10′	.4253	.9051	50'	50′	.5422	.8403	10'	10′	.6450	.7642	50′
20'	.4279	.9038	40'	33 °	.5446	.8387	57°	20′	.6472	.7623	40′
30'	.4305	.9026	30′	10′	.5471	.8371	50'	30′	.6494	.7604	30′
40'	.4331	.9013	20′	20'	.5495	.8355	40'	40′	.6517	.7585	20'
50′	.4358	.9001	10′	30′	.5519	.8339	30	50′	.6539	.7566	10′
26°	.4384	.8988	64 °	40′	.5544	.8323	20′	41°	.6561	.7547	49°
10′	.4410	.8975	50′	5 0 ′	.5568	.8307	10′	10′	.6583	.7528	50′
20'	.4436	.8962	40'	34°	.5592	.8290	56 °	20'	.6604	.7509	40'
30′	.4462	.8949	30′	10/	.5616	.8274	50′	30′	.6626	.7490	30′
40′	.4488	.8936	20′	20'	.5640	.8258	40′	40′	.6648	.7470	20′
50′	.4514	.8923	10′	30′	.5664	.8241	30/	50′	.6670	.7451	10
27°	.4540	.8910	63 °	40′	.5688	.8225	20′	420	.6691	.7431	480
10′	.4566	.8897	50′	50′	.5712	.8208	10′	10′	.6713	.7412	50′
20'	4592	.8884	40'	35°	.5736	.8192	55°	20′	.6734	.7392	40'
80/	.4617	.8870	30′	10′	.5760	.8175	50′	30′	.6756	.7373	30/
40′	.4643	.8857	20′	20'	.5783	.8158	40	40′	.6777	.7353	20′
50′	.4669	.8843	10'	30'	.5807	.8141	30/	50'	.6799	.7333	10′
280	.4695	.8829	62°	40′	.5831	.8124	20′	430	.6820	.7314	470
10′	.4720	.8816	50/	50′	.5854	.8107	10′	10′	.6841	.7294	50'
20'	.4746	.8802	40'	36°	.5878	.8090	540	20'	.6862	.7274	40′
30'	.4772	.8788	30	10′				30'	.6884	.7254	30'
40′	4797	.8774	20	20'	.5901	.8073	50/	40′	.6905	.7234	20'
50'	.4823	.8760	10′	30'	.5925	.8056	40′ 30′	50	.6926	.7214	10'
293	4848	.8746	610	40′	.5948 .5972	.8039 .8021	20	44°	.6947	.7193	46 °
				50'	.5995	.8004	10				
10' 20'	4874	.8732	50′	370	.6018	.7986	530	10′ 20′	.6967	.7173	50′ 40′
	4899	.8718	40′					30'	.7009	.7133	30'
30′ 40′	.4924 .4950	.8704 .8689	30′ 20′	10′	.6041	.7969	50′	40'	.7030	.7112	20'
50'	4975	.8675	10'	20′	.6065	.7951	40′	50′	.7050	.7092	10
				30′	.6088	.7934	30/				450
30°	.5000	-8660	60°				52°	45°	.7071	.7071	400
	4100 4	ein 4	θ		000.0	θ mis	θ	/	COR	ria o	'0 e
	$\cos \theta$	sin θ	Ø	•	cos θ	RIII Q	v	1	75.10		

Natural Tangents and Cotangents.

Φ	tan φ	etn φ		φ	tan φ	ctn φ		φ	tan φ	ctn φ	
0°	.000000		90°	7°				15°	.2679	3.732	75°
10	.002909		50′	30′	.1317	7.60	30′	10′	.2711	3.689	50′
20/	.005818		40′	40′	.1346	7.43	20′	20′	.2742	3.647	40
30′	.008727		30′	50′	1376		10′	30′	.2773	3.606	30/
40′	.011636		20′	8°	.1405	7.12	82°	40′	.2805	3.566	20/
50′	.014545		10′	10′	.1435	6.97	50′	50′	.2836	3.526	10′
1º	.017455	57.	89 °	20′	.1465	6.83	40′	16°	.2867	3.487	740
10′	.02036	49.	50′	30' 40'	.1495 .1524	6.69 6.56	30′ 20′	10′	.2899	3.450	50'
20′	.02328	43.	40′	50'	.1554	6.43	10′	20′	.2931	3.412	40′
30′	.02619	38.	30′	9°	.1584	6.31	810	30' 40'	.2962	3.376 3.340	30' 20'
40′ 50′	.02910 .03201	34. 31.	20′ 10′					50	.3026	3.305	10'
20				10′	.1614	6.197	50′	170			730
~	.03492	28.6	88°	20′ 30′	.1644	6.084 5.976	40′ 30′		.3057	3.271	
10′	.03783	26.4	50′	40′	1703	5.871	20'	10′	.3089	3.237	50'
20' 30'	.04075 .04366	24.5 22.9	40' 30'	50'	.1733	5.769	10′	20′ 30′	.3121	3.204 3.172	40' 30'
40'	.04658	21.5	20/	10°	.1763	5,671	80°	40'	.3185	3.140	20'
50′	.04949	20.2	10'	10′	.1793	5,576	50′	50'	.3217	3.108	10/
3°	.05241	19.1	870	20/	.1823	5.485	40′	180	.3249	3.078	720
10′	.05533	18.1	50′	80′	.1853	5.396	30'	10′	.3281	3.047	50′
20	.05824	17.2	40'	40′	.1883	5.309	20′	20/	.3314	3.018	40'
30′	.06116	16.3	30/	50′	.1914	5.226	10′	30′	.3346	2.989	30
40′	.06408	15.6	20'	110	.1944	5.145	79 °	40′	.3378	2.960	20/
50′	.06700	14.9	10′	10'	.1974	5.066	50/	50′	.3411	2.932	10/
4 °	.06993	14.3	86°	20'	.2004	4.989	40′	19°	.3443	2.904	71°
10′	.07285	13.73	60 ′	30′ 40′	.2035	4.915	30' 20'	10′	.3476	2.877	50′
20′	.07578	13.20	40′	50/	.2065	4.843 4.773	10'	20′	.3508	2.850	40′
30′	.07870	12.71	30′	120			780	30' 40'	.3541	2.824	30′
40′ 50′	.08163 .08456	12.25 11.83	20′ 10′		.2126			50'	.357 4 .3607	2.798 2.773	20′ 10′
5°	.08749	11.43	850	10′ 20′	.2156	4.638 4.574	50′ 40′	20°	.3640	2.747	70°
10'	.09042	11.06	50′	30′	.2217	4.511	30/	10′	.3673	2.723	50'
20	.09335	10.71	40′	40′	.2247	4.449	20/	20'	.3706	2.699	40/
30'	.09629	10.39	30′	50′	.2278	4.390	10′	30'	.3739	2.675	30'
40′	.09923	10.08	20′	13°	.2309	4.331	770	40′	.3772	2.651	20′
50′	.10216	9.79	10′	10′	.2339	4.275	50′	50′	.3805	2.628	10′
6°	.10510	9.51	840	20′	.2370	4.219	40′	21°	.3839	2.605	69 °
10′	.1080	9.26	50′	30′	.2401	4.165	30′	10′	.3872	2.583	50′
20′	.1110	9.01	40′	40′ 50′	.2432	4.113 4.061	20' 10'	20′	.3906	2.560	40′
30′	.1139	8.78	30′					30′	.3939	2.539	30/
40′ 50′	.1169 .1198	8.56 8.34	20' 10'	14°	.2493	4.011	76°	40′ 50′	.3973 .4006	2.517 2.496	20′ 10′
				10′	.2524	3.962	50′				68°
7°	.1228	8.14	83°	20′ 30′	.2555	3.914 3.867	40′ 30′	220	.4040	2.475	
10′	.1257	7.95	50′	40′	.2617	3.821	20'	10′	4074	2.455	50′
20' 30'	.1287	7.77	40' 30'	50′	.2648		10	20′ 30′	.4108 .4142	2.434 2.414	40′ 30′
30	.1317	7.60	30′ 82°	15°	.2679	3.732	750	30	4142	4.414	67°
$^{\prime\prime}$	ctn θ	tan θ	θ		ctn θ	tan θ	θ		ctn 0	tun 0	8

Natural Tangents and Cotangents.

				0.7 20.7 .5851 1.709 40.7 .7720 1.295 20.7 0.7 20.7 .5851 1.709 40.7 50.7 .7766 1.288 10.7 0.7 40.7 .5930 1.686 20.7 38.9 .7813 1.280 52.9 0.7 50.7 .5969 1.675 10.7 .7860 1.272 50.7 0.7 1.0.7 .6048 1.663 50.7 30.7 .7954 1.257 30.7 0.7 20.7 .6088 1.643 40.7 .8062 1.250 20.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8050 1.242 10.7 30.7 .8184 1.235 <td< th=""></td<>							
φ	tan φ	etn φ		φ	tan φ	ctn φ		φ	tan φ	etn φ	
220				30°	.5774	1.732	60°	37°			
30′	.4142	2.414	30′		10111			30′	.7673	1.303	30/
40'	.4176	2.394	20/							1	11
50/	.4210	2.375	10′					50′	.7766	1.288	10
230	.4245	2.356	670					380	.7813	1.280	520
10′	.4279	2.337	50′								
20'	.4314	2.318	40′	210	.8009	1.884					
30/	.4348	2.300	30/								1
40/	.4383	2.282	20								
50/	.4417	2.264	10′					50′			
240	.4452	2.246	660					39¢			
			_								I
10' 20'	.4487	2.229	50′ 40′								
30	.4522 .4557	2.211	30)
40′	4592	2.177	20′								
50	4628	2.161	10								
250	.4663	2.145	65°								11
						1					_
10′	4699	2.128	50' 40'								1
20′ 30′	.4734	2.112	30/				_				
40/	.4806	2.081	20								
50	.4841	2.066	10'								
26°	4877	2.050	640					410			1
10′	.4913	2.035	50′ 40′	_							
20′ 30′	.4950 .4986	2.020	30/								
40/	.5022	1.991	20/								1
50	.5059	1.977	10'							1	
270	.5095	1.963	63°					4000	9004	1111	480
11						1					
10' 20'	.5132	1.949	50′ 40′							1	
30′	.5206	1.921	30'							1	
40/	.5243	1.907	20					40′	.9217	1.085	20/
50′	.5280	1.894	10'	20′ 30′	.7089 .7133	1.411	40′ 30′	50'	.9271	1.079	10/
280	.5317	1.881	620	40/	.7177	1.393	20	430	.9325	1.072	470
				50′	.7221	1.385	10			 	
10′ 20′	.535 4 .5392	1.868	50' 40'	36°	.7265	1.376	54°	10' 20'	.9380 .9435	1.066	50′ 40′
30	.5430	1.842	30					30/	.9490	1.054	30/
40'	.5467	1.829	20	10' 20'	.7310	1.368	50′ 40′	40′	.9545	1.048	20/
50′	.5505	1.816	10'	30/	.7355 .7400	1.360 1.351	30/	50'	.9601	1.042	10′
290	.5543	1.804	610	40′	.7445	1.343	20'	44°	.9657	1.036	46 °
10′	,5581	1.792	50'	50′	.7490	1.335	10′	10′	.9713	1.030	50′
20'	.5619	1.782	40'	370	.7536	1.327	53°	20/	.9770	1.024	40′
30	.5658	1.767	30/				_	30/	.9827	1.018	30/
40′	.5696	1.756	20′	10′ 20′	.7581 .7627	1.319	50′ 40′	40′	.9884	1.012	20′
50′	.5735	1.744	10'	30/	.7673	1.303	30'	50′	.9942	1.006	10′
30°	.5774	1.732	600	اٽا			52°	450	1.0000	1.000	450
			L				3~		1-		
'/ /	ctn θ	tan θ	θ		ctn θ	tan 0	θ	1	ctn	at O	10 6
/ I					1			•	1		

Natural Secants and Cosecants.

φ	ве с ф	csc φ		φ	sec φ	csc φ		φ	ser.∲	свс ф	
0°	1.0000		90°	7°				15°	1.035	8.864	75°
10′	1.0000	}	50′	30′				10′	1.036	3.822	50′
20′	1.0000		40′	50'							1
30′	1.0000		30′	80				1			
40′ 50′	1.0001	! !	20′ 10′					50'			
10	1.0002	57.	890	20'			40'	16°			740
10′	1.0002	49.	50′	30′	1.011	6.77	30′	10	1.041	8.592	50/
20	1.0003	43.	40	40′	1.012	6.64		20	1,042	3.556	1
30'	1.0003	38.	30'	50′	1.012	6.51		30′	1.043	3.521	30/
40′	1.0004	34.	20′	9 °	1.012	6.39	81 °		1.044		
50′	1.0005	31.	10′	10′	1.013	6.277	50′	_	1.045		1
2°	1.0006	28.7	880	20′	1.013	6.166		179	1.046	3.420	73°
10'	1.0007	26.5	50′	30′				10'	1.047	3.388	50′
20′	1.0008	24.6	40′	50							40'
30′	1.0010	22.9	30′								
40′ 50′	1.0011	21.5 20.2	20′ 10′			-					
3°	1.0014	19.1	870	20'				180			
10′	1.0015	18.1	50′	30′	1.017	5.487	30′				
20	1.0013	17.2	40′	40′	1.018	5.403	20′				
30/	1.0019	16.4	30	50′	1.018	5.320	10′	30	1.054	3.152	30/
40′	1.0021	15.6	20′	110	1.019	5.241	79 °	4()	1.056	3.124	20′
50′	1.0022	15.0	10′	10′	1.019	5.164	5 0′	50	1.057	3.098	10′
4 °	1.0024	14.3	86°	20′	1.020	5.089	40′	19°	1.058	3.072	710
10/	1.0026	13.76	50′	40'				10'		1	50′
20/	1.0029	13.23	40′	50'							
30' 40'	1.0031	12.75 12.29	30′ 20′	120							
50'	1.0036	11.87	10	10'				50	1.063	2.947	10
5 °	1.0038	11.47	85°	20′	1.024	4.682	40′	500	1.064	2.924	700
10	1.0041	11.10	50′	30′		4.620	30′	10′	1.065	2.901	50′
20'	1.0043	10.76	40′	40′				20′	1.066	2.878	40′
30/	1.0046	10.43	30′					80	1.068	2.855	30/
40' 50'	1.0049	10.13	20′	13°							
6°	1.0052	9.84	10′ 84•	10′	1.027	4.390	50′				8
11 - 1				30'							
10' 20'	1.0058 1.0061	9.31 9.07	50′ 40′	40′	1.029	4.232	20				
30'	1.0065	8.83	30	50′	1.030	4.182	10				
40'	1.0068	8.61	20'	140	1.031	4.134	760	40'	1.076	2.709	20/
50′	1.0072	8.40	10′	10′			50	50′	1.077	2.689	10′
70	1.0075	8.31	83 °	20′	1.032	4.039	40	220	1.079	2.669	68 °
10′	1.0079	8.02	50′	30′	1.033	3.994	30′	10′	1.080	2.650	50'
20′	1.0082	7.83	40′	40′ 50′				20′	1.081	2.632	40'
30′	1.0086	7.66	30′					30′	1.082	2.613	30′
//			82°	15°	1.009						
	csc 0	sec 0	θ		ese θ	sec 0	θ		C8C 0	800 8	9 (

Natural Secants and Cosecants.

_											
ψ	вес ф	свс ф		φ	sec φ	свс ф		φ	sec φ	свс ф	
220				30 °	1.155	2.000	60 °	37 °			
30/	1.082	2.613	30′	10′	1,157	1.990	50′	30/	1.260	1.643	30/
40′	1.084	2.595	20′	20	1.159	1.980	40/	40′	1.263	1.636	20'
50'	1.085	2.577	10′	30'	1,161	1.970	30/	50′	1.266	1.630	10'
23°	1.086	2.559	670	40′	1.163	1.961	20'	380	1.269	1.624	52 °
10	1.088	2.542	50′	50′	1.165	1.951	10′	10′	1,272	1.618	50′
20′	1.089	2.525	40'	31°	1.167	1.942	59°	20′	1.275	1.612	40/
30′	1.090	2.508	30/	10′	1.169	1.932	50'	30′	1.278	1.606	30/
40'	1.092	2.491	20'	20'	1.171	1.923	40	40′	1.281	1.601	20'
50'	1.093	2.475	10/	30'	1.173	1.914	30	50′	1.284	1.595	10'
240	1.095	2.459	660	40′	1.175	1.905	20	39°	1,287	1.589	51 °
10′	1.096	2.443	50'	50′	1.177	1.896	10'	10′	1.290	1.583	50′
20	1.097	2.427	40/	32 °	1.179	1.887	580	20	1.293	1.578	40′
30	1.099	2.411	30/					30	1.296	1.572	30/
40'	1100	2,396	20'	10′	1.181	1.878	50′	40′	1.299	1.567	20'
50	1102	2,381	10'	20′	1.184	1.870	40′	50'	1.302	1.561	10
250	1.103	2,366	65°	30′ 40′	1.186	1.861	30' 20'	40°	1,305	1.556	500
10	1.105		50′	50'	1.190	1.844	10	10′		 	
20'	1.106	2.352 2.337	40'	330	1.192	1.836	570	20/	1.309	1.550	50′ 40′
80/	1.108	2.323	30/				_	80′	1.315	1,540	30
40′	1.109	2.309	20	10′	1.195	1.828	50′	40′	1.318	1.535	20'
50	1.111	2.295	10	20′	1.197	1.820	40′	50′	1.322	1.529	10′
26°	1.113	2,281	640	30′ 40′	1.199	1.812	30' 20'	410	1,325	1.524	490
				50′	1.204	1.796	10			+	
10′	1.114	2.268	50′				560	10′	1.328	1.519	50′
804	1.116	2.254	40′	3 4 °	1.206	1.788		20′ 30′	1.332	1.514	40′
30' 40'	1.117	2.241	30′	10′	1.209	1.781	5 0 ′		1.335	1.509	30′
90	1.119	2.228	20′	20′	1.211	1.773	40′	40′ 50′	1.339 1.342	1.504	20′ 10′
		2.215	10′	30′	1.213	1.766	30′			1.499	• 1
27"	1.122	2.203	63°	40′ 50′	1.216	1.758	20' 10'	4 2°	1.346	1.494	48°
10	1.124	2.190	50′				ı	10′	1.349	1.490	50′
20′	1.126	2.178	40′	35°	1.221	1.743	55°	20′	1.353	1.485	40′
80′	1.127	2.166	30/	10′	1.223	1.736	50′	30′	1,356	1.480	30′
40′	1.129	2.154	20′	20′	1.226	1.729	40′	40′	1.360	1.476	20′
50′	1.131	2.142	10′	30′	1.228	1.722	30′	50'	1.364	1.471	10′
28°	1.133	2.130	62°	40′	1.231	1.715	20′	43°	1.367	1.466	47°
10′	1.134	2.118	50′	50′	1.233	1.708	10′	10′	1.371	1.462	50′
20′	1.136	2.107	40′	36°	1.236	1.701	54°	20′	1.375	1.457	40′
30′	1.138	2.096	30′	10′	1.239	1.695	50′	30′	1.379	1.453	30′
40′	1.140	2.085	20′	20'	1.241	1.688	40/	40′	1.382	1.448	20′
50′	1.142	2.074	10′	30′	1.244	1.681	30/	5 0′	1.386	1.444	10′
29°	1.143	2.063	61°	40′	1.247	1.675	20′	44°	1.390	1.440	4 6°
10′	1.145	2.052	50'	50′	1.249	1.668	10′	10′	1.394	1.435	50′
20′	1.147	2.041	40′	37 °	1.252	1.662	53°	20′	1.398	1.431	40′
30′	1.149	2.031	30'	10′	1.255	1.655	50′	30′	1.402	1.427	30′
40'	1.151	2.020	20'	20/	1.258	1.649	40′	40′	1.406	1.423	20′
50′	1.153	2.010	10′	30'	1.260	1.643	30′	50′	1,410	1.418	10′
30 °	1,155	2.000	60°				520	45°	1.414	1.414	(45 0
								1	$\overline{}$. 8
' <i> </i>	csc θ	sec θ	θ		csc θ	86C 0	θ	1	/ csc	θ <i>86</i> 0	. 0 .
					1						

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EXPLANATION OF THE TABLES.

§ 1. TABLES IN GENERAL.

- a. One quantity is said to be a function of another, when the former quantity is regarded as determined by the latter, according to some rule or formula. E. g. x^2 , \sqrt{x} , $\log x$, $\sin x$, $\log \sin x$, are all called functions of x. A mathematical table is an orderly arrangement of the values of some function for certain selected values of the quantity by which it is regarded as determined. The successive values of the latter quantity are assumed arbitrarily, and generally at equal intervals; and this quantity is called the argument of the table. Some functions require several independent quantities for their determination; and the corresponding tables are tables of several arguments. Thus, a multiplication-table is a table of two arguments; namely, the two factors.
- b. A table may be used in two ways: directly and inversely. The direct use of the table consists in finding the value of the function for an assumed value of the argument; the inverse use, in finding the value of the argument for an assumed value of the function.
- c. Before beginning to use any table, the student should give attentive consideration to its arrangement, and to the best mode of employing it with accuracy and ease. Every feature of it should be carefully examined, and the explanations which are attached to it should be fully mastered. The time thus spent will be time gained, contributing not only to power in computation, but also, very materially, to the thorough practical knowledge of the nature of the tabulated functions.

§ 2. INTERPOLATION.

a. Interpolation consists in finding the value of one of the two quantities, argument and function, for an assumed value of the other quantity, lying between two successive tabulated values. Most mathematical tables are so constructed as to admit of interpolation by the principle that corresponding non-tabulated values of the function and argument lie between corresponding tabulated values and divide the differences between them in the same ratio. This is the principle of proportional parts. Let x_1 and x_2 be two successive tabulated values of the argument of a table, and u_1 and u_2 the correspond-

ing values of the function. Then, $x_2 - x_1$ and $u_2 - u_1$ are called corresponding tabular differences. We shall denote these differences by Δx and Δu . If, now, x and u are corresponding values of the function and argument, of which one is known to lie between the two above-cited tabulated values of the same quantity, the principle of proportional parts is that if

$$\lambda = \frac{x - x_1}{\Delta x}, \qquad \lambda' = \frac{x_2 - x}{\Delta x} = 1 - \lambda.$$

$$\mu = \frac{u - u_1}{\Delta u}, \qquad \mu' = \frac{u_2 - u}{\Delta u} = 1 - \mu,$$

then (to the limit of accuracy belonging to the table)

or,
$$\lambda = \mu, \qquad \lambda' = \mu',$$
$$u = u_1 + \lambda \Delta u = u_2 - \lambda' \Delta u,$$
$$x = x_1 + \mu \Delta x = x_2 - \mu' \Delta x.$$

Thus, the required value of the function or argument may be obtained by applying a correction to either of the two tabulated values between which the required value lies. In computing this correction, the signs of the differences employed must be carefully observed. If x_1 and x_2 are so chosen as to make Δx positive, Δu may be either positive or negative. In the former case, the function is said to be increasing; in the latter, decreasing.

- b. Either of the two formulas given above for finding u may be employed, in interpolation, in the direct use of the table; either of the formulas for x may be employed in the inverse use of the table. In most tables, $\Delta x =$ one unit in the last numeral place of the tabulated values of x. Hence λ is composed of the figures which follow that numeral place in the given non-tabulated value of the argument, preceded by a decimal-point; while λ' is the complement of λ (that is, can be found by subtracting from 9 each figure of λ except the last, and subtracting that from 10). The correction for u is, therefore, found simply by multiplying the figures in question into Δu , and pointing off according to the case; x will be corrected by annexing to x_1 the figures of $\frac{u-u_1}{\Delta u}$, or the figures complementary to $\frac{u_2-u}{\Delta u}$.
- c. In some of the tables of this collection will be found, set against each value of the function, a number in small type, which shows what Δu would be if the function varied through a whole interval corresponding to Δx at the same rate at which it is changing when it passes through the value against which this number is set. This number may be called the rate of difference, or simply the difference, of u, and may be substituted for Δu in the formulas of interpolation. But, in that case, we ought to work from the nearest tabulated value of x or u; that is, from x_1 or u_1 when λ or $\mu < 0.5$, and from x_2 or u_2 when λ' or $\mu' < 0.5$. (See examples in the explanation of the table of Logarithms of Circular Functions.)
- d. An interpolated value of the function should not be carried out beyond the last numeral place of the tabulated value from which it is computed; so that, in finding $\lambda \Delta u$ or $\lambda' \Delta u$, we should reject the decimal part of the product, Δu being regarded as an integer. Owing to the combination of the figures rejected in the correction and those omitted in the tabulated value of the function, an interpolated value is liable to an error of ± 1 in the last figure.

Proportional Parts.

The number of figures annexed to the tabulated value of the argument, in inverse interpolation, should be less by one than the number of figures contained in Δu . It is sometimes, indeed, made equal to the latter number (and will always be, if Δu consists of only one figure); but, in that case, the last figure must be regarded as uncertain. When the given value of the function is the result of computation, of course this uncertainty may extend back to earlier figures.

e. In taking the correction of either the function or the argument only to a certain number of figures, we must observe the following rule, which is a universal rule of computation:—

Whenever figures are neglected at the end of a number, if the figures neglected amount to more than half a unit in the place of the last figure retained, the last figure retained must be increased by 1. E. g. 27.528 = 27.53 to the nearest hundredth = 27.5 to the nearest tenth = 28 to the nearest unit = 80 to the nearest ten.

f. The various rules of interpolation will be found to be fully exemplified below, in the explanations of the tables of Logarithms and Logarithms of Circular Functions.

g. In interpolating in some tables (e. g. in VLACQ's great ten-place table), we must have regard to **second differences**, or differences between differences. In this case, we add to the above formulas for u the term

$$-\frac{1}{2}\lambda\lambda'\Delta^2u$$

where $\Delta^2 u$ denotes the second difference of u, taken positively when Δu is increasing. The greatest value of this term is one eighth of $\Delta^2 u$, so that it is insignificant when $\Delta^2 u < 4$. In the present tables this term may always be neglected; although it is useful as measuring the extent of error, and may occasionally guide the judgment of the computer when the fractional part of the correction is equal, or nearly equal, to 0.5. But where such nicety of work seems to be called for, it is best to use a table of a larger number of places.

§ 3. PROPORTIONAL PARTS.

a. The table of **Proportional Parts** (folded page) may be used in connexion with any other table, as an aid in interpolation. It contains the product of every integer from 1 to 100 by every tenth from 0.1 to 0.9. If the multiplier consists of one figure in any other numeral place, it is only necessary to change the position of the decimal-point in the product. To multiply a number of two figures by any decimal whatever, we must find the products which correspond to the successive figures of the multiplier, and add them together. The decimal part of the result is generally to be discarded, and in that case the general rule given above (in § 2, e) must be observed. Thus, let it be required to find 0.619 \times 37. Looking in the column belonging to 37, we find

$$0.6 \times 37 = 22.2$$

 $0.01 \times 37 = 0.37$
 $0.009 \times 37 = 0.333$
 $0.619 \times 37 = 23$

In like manner, we find

$$0.27 \times 15 = 4$$
, $0.59 \times 73 = 43$, $0.78 \times 69 = 54$, $0.96 \times 84 = 81$, $0.36 \times 57 = 21$, $0.289 \times 51 = 15$, $0.483 \times 93 = 45$, $0.374 \times 82 = 31$, $0.053 \times 68 = 4$.

b. This table can also be used inversely. Thus, let it be required to find, to two decimal-places, what part 36 is of 79. Looking in the column of 79, we find

$$0.4 \times 79 = \frac{36}{4.4}$$

$$0.06 \times 79 = 4.74 \text{ (the nearest product)}$$

$$\therefore \frac{36}{79} = 0.46.$$

In like manner, we find

$$\frac{29}{68} = 0.43, \quad \frac{72}{89} = 0.81, \quad \frac{31}{98} = 0.32, \quad \frac{26}{71} = 0.37, \quad \frac{45}{57} = 0.79, \quad \frac{11}{37} = 0.30.$$

A little practice will enable the student to use this table easily and rapidly.

§ 4. LOGARITHMS.

- a. Denary, or Briggsian, logarithms, being those employed in actual computation, are always referred to, in this collection of tables, when the term logarithm is used without qualification. The characteristic, or integral part, of the denary logarithm of a number depends only on the position of the first significant figure of the number relatively to the units' place, and may be found by a well-known rule; the mantissa, or fractional part, depends only on the series of significant figures which compose the number, and is the only part of the logarithm for which it is necessary to employ a table. A table of logarithms is complete, to an assigned number of places, if it gives (explicitly or by interpolation) to that number of places the mantissa of the logarithm of every possible series of significant figures. Denary logarithms are, in general, incommensurable numbers, and cannot, therefore, be exactly expressed in They are variously given, in different tables, to ten, seven, six, five, four, and three places of decimals. Four-place logarithms are sufficient for the ordinary purposes of engineering, navigation, the work of the physical and chemical laboratory, and many of the subordinate computations of astronomy; and, in most of these cases, are all that the accuracy of the data will justify us in using. Seven places are, however, needful for the more accurate kinds of astronomical and geodetic work.
- b. If one number is the logarithm of another, the second number is called the antilogarithm of the first. This relation is denoted by the symbol log^{-1} . Thus, if u = log x, then $x = log^{-1} u$. In an ordinary table of logarithms, the argument is the antilogarithm, which is tabulated to a greater or less number of figures, according to the number of places to

Logarithms.

which the logarithm is given, and the function is the mantissa of the logarithm, which we often speak of simply as the logarithm.

To find the logarithm of any number.

c. If the number consists of three significant figures, seek the first two significant figures in the first column of the table of Logarithms (pp. 2, 3), and the third at the top of the table. In the line and column thus determined will be found the mantissa of the required logarithm, printed without the decimal-point. Find the characteristic by the rule, and prefix it, with the decimal-point, to the mantissa. E. g., log 2870 = 3.4579. If the given number has less than three significant figures, fill it out to three figures by anexing a zero or zeros. E. g., $\log 0.35 = \log 0.350 = 9.5441 - 10$. $\log 6 = \log 6.00 = 0.7782$. If the number has more than three significant figures, its logarithm must be found by one of the formulas of interpolation given above. The rule is: - Find the logarithm of the first three significant figures of the given number and also that of the next following number of three figures (1000 following 999); then apply to EITHER of these two logarithms a correction, obtained by multiplying the difference between them by the difference between the given number and the three-figure number which corresponds to the logarithm chosen to be corrected, and rejecting (with due attention to the rule of § 2, e) as many figures at the end of the product as are contained in the latter difference. The table of Proportional Parts may be employed in performing the multiplications. Thus, to find log 5668.4. Using the notation of the formulas of interpolation, and remembering that the place of the decimal-point in the given number may be disregarded in finding the mantissa of the required logarithm, we have

$$x_1 = 566,$$
 $u_1 = \text{mant log } x_1 = 7528,$ $x_2 = 567,$ $u_2 = \text{mant log } x_2 = 7536,$ $\Delta x = 1,$ $\Delta u = 8;$

so that log x may be found by either of the following methods: —

$$\lambda = 0.84$$
, $\lambda \Delta u = 6.72 = 7$ to units, $u = 7528 + 7 = 7535$; or, $\lambda' = 1 - \lambda = 0.16$, $\lambda' \Delta u = 1.28 = 1$ to units, $u = 7536 - 1 = 7535$.

 $\log 5668.4 = 3.7535.$

Let the beginner find the following logarithms by this method: -

```
    log 59.43
    = 1.7740,
    log 0.0081472
    = 7.9110
    10,

    log 284.8
    = 2.4545,
    log 572820
    = 5.7581,

    log 0.073748
    = 8.8678
    10,
    log 0.50167
    = 9.7004
    10,

    log 3.1607
    = 0.4998,
    log 99968,
    = 4.9999.
```

The interpolated logarithm should never be carried to more than four decimalplaces.

d. The work of interpolation may be shortened by using the column of proportional parts, marked P. P., on the right of the table. In using this column, one must work from the three-figure number NEAREST to the given

number (in the above example, from 567, not from 566). If the given number has only four figures, so that λ or λ' has only one figure, then the correction will be found in the column P. P., under λ or λ' (according as we are working from the number below or the number above the given number), and in the same line with the logarithm to be corrected. If the given number has more than four figures, the correction must be estimated by the observation of the corrections which correspond to the figures below and above the first figure of λ or λ' . E. g.

```
mant log 2848 = mant log 285 — cor. for .2 = 4548 — 3 = 4545; mant log 56684 = mant log 567 — cor. for .16 = 7536 — 2 = 7534
```

In the last case the correction is either 1 or 2, and, since .16 is nearer .20 than .10, we choose the correction belonging to .20. Larger tables show that the mantissa of the required logarithm, to five places, is 75346; so that the value found by the column P. P. is here nearly as accurate as that obtained by computation. There is a slightly greater liability to error when we use the column P. P. than when we interpolate by computation; but the disadvantage is generally insignificant. The last figure of an interpolated logarithm obtained from any table may always be one unit in error. E. g.: the true mant log of 57282 to five places is 75802; and this is a case in which the column P. P. gives a better result than computation.

The student is advised now to find all the logarithms in the above list by using the column P. P.

e. If the first figure of the given number is 1, it will be found tabulated to four figures in pp. 4, 5. The correction for a fifth and following figures may be found by the method of interpolation explained in c. As the differences are always small on these pages, and the corrections easily computed, the column P. P. is not here given; but, to facilitate taking the last difference, we have printed at the end of each line, under the heading 10, the first logarithm of the following line. Let the student find the following logarithms:—

```
\log 11.737 = 1.0696, \log 0.00100066 = 7.0003 - 10, \log 0.15703 = 9.1960 - 10, \log 18597. = 4.2694.
```

To find the antilogarithm of any logarithm.

f. It is enough to explain the way of finding the series of significant figures which compose the antilogarithm, by means of the mantissa of the given logarithm; the pointing off of the antilogarithm being determined, according to rule, by the given characteristic. If the mantissa of the given logarithm is contained in the table, the required antilogarithm is at once found by inspection. Otherwise, we must resort to the formulas of interpolation, which give the following rule: — Find two successive tabulated logarithms $(u_1 \text{ and } u_2)$ between which the given logarithm (u) lies; then divide the difference between either of these tabulated logarithms and the given loyarithm $(u - u_1 \text{ or } u_2 - u)$ by the difference between the tabulated logarithms (Δu) , carry out the quotient to the NEAREST tenth (that is, to one figure, which may be 0), and add it to or subtract it from the antilogarithm $(x_1 \text{ or } x_2)$ of the tabulated logarithm $(u_1 \text{ or } u_2)$ with which the given loyarithm has been compared. The antilogarithm is always a figure annexed to the three or four tabulated figures of x_1 .

Logarithms of Sums and Differences.

The division should not generally be carried beyond one figure. Even the first figure is, in most cases, somewhat uncertain. If the mantissa of the given logarithm is less than 3010, pp. 4, 5 should be used. On pp. 2, 3, the column P. P. may be employed.

Let it be required to find log-1 1.5284. We find

$$u_1 = 5276,$$
 $x_1 = 337,$ $u - u_1 = 8,$ $u_2 - u = 5,$ $u_2 = 5289,$ $x_2 = 338,$ $\mu = \mu \Delta x = \frac{8}{13} = 0.6..,$ $\Delta u = 13,$ $\Delta x = 1,$ $\mu' = \mu' \Delta x = \frac{5}{13} = 0.4..,$ $x = 337 + 0.6 = 338 - 0.4 = 337.6;$ $\therefore \log^{-1} 1.5284 = 33.76.$

More briefly, looking along the line of $u_2 = 5289$ for $5 = u_2 - u$ in column P. P., we find that 5 corresponds to the correction 4, which gives at once the required number. In like manner, the student may find

$$\begin{array}{lll} \log^{-1} \ 1.9155 = 82.32, & \log^{-1} \ (5.8760 - 10) = 0.00007517, \\ \log^{-1} \ 3.8291 = 6747, & \log^{-1} \ (9.5727 - 10) = 0.3738, \\ \log^{-1} \ 0.1548 = 1.4283, & \log^{-1} \ (8.2731 - 10) = 0.018755. \end{array}$$

g. The convenient usage of making negative characteristics positive, by the addition of 10, is followed, throughout the present collection of tables, whenever logarithms are printed with their characteristics. This must be always understood, though no explicit reference be made to it in the explanation of the table.

§ 5. LOGARITHMS OF SUMS AND DIFFERENCES.

a. This is one form of a table devised by Gauss to facilitate finding the logarithm of the sum or difference of two numbers which are themselves given only by their logarithms. The argument of the table is any logarithm, and may be called $\log x$; the function tabulated is then $\log (x+1)$. It follows that, if the function is denoted by $\log x$, the argument is $\log (x-1)$. The function may be called the **Gaussian** of the argument, and the argument the anti-Gaussian of the function; and the symbols G and G^{-1} may be used to denote these relations. Thus we have

$$\log (x+1) = \mathfrak{G} \log x, \qquad \log (x-1) = \mathfrak{G}^{-1} \log x.$$

b. To find the Gaussian of a given logarithm. Seek the characteristic of the given logarithm (increased by 10 if negative) at the top of the table, and the first two figures of the mantissa in the left-hand column. If the third and fourth figures of the mantissa are zero, the Gaussian will be found in the column and line thus determined; otherwise, it can be obtained by the method of interpolation which has been fully explained in § 2. In three columns of the table, the rate of difference of the Gaussian is printed in small type after the value of the function, and may be used instead of the tabular difference of the Gaussian through half the tabular interval before and after the value to which it is attached, as explained in

§ 2, c, and completely illustrated below, in the explanation of the table of Logarithms of Circular Functions. The table of Proportional Parts may be employed in computing the corrections. Examples:—

(3)
$$1.0960 = 1.1295$$
,
 (3) $(7.5265 - 10) = 0.0015$,

 (3) $3.8129 = 3.8130$,
 (3) $(9.6431 - 10) = 0.1582$.

 If $\log x < 6.0000 - 10$,
 $\log (x + 1) = 0.0000$ to four places;

 if $\log x > 4.0000$,
 $\log (x + 1) = \log x$ to four places.

c. To find the anti-Gaussian of a given logarithm. Seek, in the body of the table, two successive logarithms between which the given logarithm lies, and then find the corresponding value of the argument by interpolation. Examples:—

$$\mathfrak{G}^{-1}$$
 1.0960 = 1.0597, \mathfrak{G}^{-1} 0.1051 = 9.4373 — 10, \mathfrak{G}^{-1} 3.8129 = 3.8128, \mathfrak{G}^{-1} 1.0216 = 0.9782.

d. To find the logarithm of the sum or difference of the antilogarithms of two given logarithms. If m and n are two numbers,

$$m+n=n\left(\frac{m}{n}+1\right), \qquad m-n=n\left(\frac{m}{n}-1\right),$$

$$\log (m+n)=\log n+\log \left(\frac{m}{n}+1\right)=\log n+\Im \log \frac{m}{n},$$

$$\log (m-n)=\log n+\log \left(\frac{m}{n}-1\right)=\log n+\Im \log \frac{m}{n}.$$

Example: —

Given
$$a=4.142$$
, $b=2.399$; to find $\sqrt{(a^2+b^2)}$ and $\sqrt{(a^2-b^2)}$.
 $\log a = 0.6172$, $\log b = 0.3800$, $\log a^2 = 1.2344$, $\log b^2 = 0.7600$, $\log \frac{a^2}{b^2} = 0.4744$;
 $\Im \log \frac{a^2}{b^2} = 0.6000$, $\Im \log \frac{a^2}{b^2} = 0.2970$, $\log b^2 = 0.7600$, $\log b$

§ 6. CIRCULAR, OR TRIGONOMETRIC, FUNCTIONS: NATURAL VALUES.

a. Three tables of the natural values of the trigonometric functions are given on pp. 22-27. Each table is broken up into six divisions, and occupies two pages. The argument is the angle, which is tabulated at intervals of 10' from 0° to 90°. Angles in the first half of the quadrant will be found in the left-hand column of the several divisions of the table, and for those angles the names of the functions are to be taken from the top of the page; angles in the second half of the quadrant are to be found in the right-hand.

Logarithms of Circular Functions.

column of the table, and for those angles the names of the functions are to be taken from the bottom of the page. The angles standing at the right and left in the same line are complements of each other; and the names of the functions at the top and bottom of the same column are complementary. The value of any of the functions for a non-tabulated angle, or the value of the angle for a non-tabulated value of one of the functions, can be found by the method of interpolation explained in § 2. The precepts of § 2, d, e, should be observed in computing the corrections. The tabulated values of the functions are generally given to four significant figures; but, in the tables of tangents and secants, they are sometimes given to a less number of figures (to avoid errors in interpolation), and are sometimes omitted altogether. In these cases the functions can be best found by finding their logarithms by the table of Logarithms of Circular Functions (see § 7), and then the numbers corresponding by the table of Logarithms.

b. To find any function of an angle greater than 90°, we must subtract from the given angle the greatest multiple of 90° which it contains; if an even multiple has been subtracted, we look out the required function of the remainder; if an odd multiple, the complementary function; and we then fix the sign of the function by considering the quadrant in which the given angle lies. For a negative angle, we find the required function of the corresponding positive angle, and then fix its sign by considering the quadrant of the angle.

c. Examples of the use of these tables: -

```
sin 77° 37'
                                   \tan 53^{\circ} 04' = 1.330
                        0.9767.
                                                                     \sec 68^{\circ} 45' =
                                                                                             2.759,
                        0.9597,
cos 16° 19'
                                    ctn
                                            3^{\circ} 18' =
                                                           17.4,
                                                                     \csc 55^{\circ} 13' =
                                                                                             1.217;
                                                                     sec 325° 13' =
                                                                                             1.217,
\sin 257^{\circ} 37' = -0.9767, \tan 93^{\circ} 18' = -17.4,
\cos 163^{\circ} 41' = -0.9597, \cot 323^{\circ} 04' = -1.330, \csc 158^{\circ} 45' =
                                                                                             2.759;
\sin(-257^{\circ}37') = 0.9767, \tan(-93^{\circ}18') = 17.4, \sec(-325^{\circ}13') =
\cos(-163^{\circ}41') = -0.9597, \cot(-323^{\circ}04') = 1.330, \csc(-158^{\circ}45') = -2.759;
      \sin^{2} 0.2000
                                  11^{\circ} 32' \text{ or } = 168^{\circ} 28' \text{ or } =
                                                                            371° 32′, etc.,
      \cos^{-1}(-0.3542) = 110^{\circ} 45' \text{ or } = 249^{\circ} 15' \text{ or } =
                                                                            830° 45′, etc.,
      tan^{-1} (-4.570) = 102° 21′ or = 282° 21′ or = -77° 39′, etc.,
                                   72^{\circ} \ 27' \text{ or } = 252^{\circ} \ 27' \text{ or } = -107^{\circ} \ 33', \text{ etc.},
      ctn-1 0.3163
      sec-1 5.000
                                   78^{\circ} 28' \text{ or } = -78^{\circ} 28' \text{ or } = \pm 281^{\circ} 32', \text{ etc.},
      \csc^{-1} (-3.529) = -16° 28′ or = 196° 28′ or = -163° 32′, etc.
```

§ 7. LOGARITHMS OF CIRCULAR FUNCTIONS.

To find the logarithm of any circular function of a given angle.

a. If the angle is less than 6° , the part of the table which occupies the upper half of p. 10 may be used. (See also g.) The left-hand division of this part of the table gives the values of a logarithm S (the characteristic and the first two figures of the mantissa being printed at the head of the column), with the angular limits between which each value may be used. Thus, for all positive angles less than 1° 51'.479, S = 6.4637; for all angles between 1° 51'.479 and 2° 49'.567, S = 6.4636; etc. The next following

division gives, in like manner, the values of a logarithm T. We must find the logarithm of the angle, reduced to minutes and decimals of a minute, and must then apply the formulas:—

```
\log \sin \phi = \log (\phi \text{ in minutes}) + S - 10,

\log \tan \phi = \log (\phi \text{ in minutes}) + T - 10.
```

The two right-hand divisions of this part of the table give the values of the log sec, with the angular limits for each value. The logarithms of the cosine, cotangent, and cosecant are the arithmetical complements (— 10) of the logarithms of the secant, tangent, and sine, respectively. Example:—

```
\begin{array}{l} 1 \sin 3^{\circ} 15'.23 = 8.7541, \quad 1 \tan 3^{\circ} 15'.23 = 8.7548, \quad 1 \sec 3^{\circ} 15'.23 = 0.0007, \\ 1 \csc 3^{\circ} 15'.23 = 1.2459, \quad 1 \cot 3^{\circ} 15'.23 = 1.2452, \quad 1 \cos 3^{\circ} 15'.23 = 9.9993; \end{array}
```

the negative characteristics being here, as in the following examples, made positive by the addition of 10.

b. If the angle is acute and greater than 84°, we must take its complement, and then seek the function complementary to that required, for the angle thus obtained, by the method just expounded. Example:—

```
l sin 86° 44′.77 = 9.9993, l tan 86° 44′.77 = 1.2452, l sec 86° 44′.77 = 1.2459, l csc 86° 44′.77 = 0.0007, l ctn 86° 44′.77 = 8.7548, l cos 86° 44′.77 = 8.7541.
```

c. If the angle is contained between 6° and 84°, we use the main part of the table, occupying the lower half of p. 10 and pp. 11-15. The angle is tabulated at intervals of 10', from 6° to 45° in the left-hand column of the table, and from 45° to 84° in the right-hand column. The names of the functions are to be taken from the tops of the columns, when the angle is on the left; and from the bottoms of the columns, when the angle is on the right. The angles on the right and left of any line and the names at the top and bottom of any column have the same relation to each other as in the tables of Natural Values (§ 6). The true characteristic in the first, third, and sixth columns is -1, but is printed 9. The six columns are arranged in pairs. The two functions in each pair of columns are reciprocal to each other; and the logarithms are therefore complementary, and their differences are equal in value, with opposite signs. Down the middle of each double column are printed, in small type, the rates of difference of the logarithms in that double column. Each value of this rate may be used in interpolation, instead of Δu , through half the interval before and after the line on which it stands, as stated in § 2, c. Thus, in finding the logarithms of the circular functions of any angle between 25° 25' and 25° 35' we work from the values corresponding to 25° 30', the nearest tabulated angle; and compute the corrections by taking proportional parts of 26, 33, and 6, for the three pairs of functions. In applying the corrections, we must carefully observe, for each function, whether the function is increasing or decreasing.

For example, let the logarithms of the circular functions of 25° 27'.4 = 25° 30' — 02'.6 be required. We find

Logarithms of Circular Functions.

In like manner, we have

$$1 \sin 74^{\circ} 46' = 9.9845$$
, $1 \tan 74^{\circ} 46' = 0.5849$, $1 \sec 74^{\circ} 46' = 0.5804$, $1 \csc 74^{\circ} 46' = 0.0155$, $1 \cot 74^{\circ} 46' = 9.4351$, $1 \cos 74^{\circ} 46' = 9.4196$.

d. If the angle is greater than 90° , or negative, we must use the method explained in § 6, b, for the tables of Natural Values of the circular functions. When the natural value of a circular function is negative, this should be indicated by writing the letter n after its logarithm. Examples:

```
l sin 105° 14′ = 9.9845, l tan 105° 14′ = 0.5649 n, l sec 105° 14′ = 0.5804 n, l csc 164° 46′ = 0.5804, l ctn 164° 46′ = 0.5649 n, l cos 164° 46′ = 9.9845 n, l sin (-74^{\circ} 46′) = 9.9845 n, l tan (-105^{\circ} 14′) = 0.5649, l cos (-394^{\circ} 46′) = 9.4196.
```

Given the logarithm of any circular function, to find the value of the corresponding angle.

e. If the given logarithm lies without the limits of the main part of the table, the upper part of p. 10 may be used. If the given logarithm is a log sin less than 9.0192, or a log tan less than 9.0216, subtract from it the proper value of S or T (or add the arithmetical complement), and the remainder is the log of the required angle in minutes. The limiting values of the log sin and log tan for each value of S and T are given in the table. If the given log is a log csc greater than 0.9808, or a log ctn greater than 0.9784, its arithmetical complement will be a log sin less than 9.0192, or a log tan less than 9.0216. If the given log is a log sec less than 0.0024, the limits between which the required angle lies are given by the table; the angle may have any value between these limits, and is not therefore very closely determined. If the given log is a log cos greater than 9.9976, its arithmetical complement is a log sec less than 0.0024.

If the given log is a log sin, log tan, or log sec greater than 9.9976, 0.9784, or 0.9808 (respectively), or a log csc, log ctn, or log cos less than 0.0024, 9.0216, or 9.0192 (respectively), we must change the name of the function to the complementary name (sin to cos, etc.), find the corresponding angle as above, and take the complement of the angle thus found. Examples:—

$$(\log \sin)^{-1} 8.9542 = 5^{\circ} 09'.8,$$
 $(\log \cot)^{-1} 2.0531 = 0^{\circ} 30'.42,$ $(\log \cot)^{-1} 9.0024 = 84^{\circ} 15'.5,$ $(\log \sin)^{-1} 9.9983 = 84^{\circ} 56' \pm 4\frac{1}{2}'.$

f. If the given logarithm is contained within the limits of the main part of the table, the required angle is found by ordinary interpolation; and we may use the printed rate of difference as the value of Δu , working in each case from the nearest tabulated value. The angle should be found to the nearest minute, or, when the difference exceeds 100, to the nearest tenth of a

minute. But in the right-hand pair of columns, the last figure of the angle thus found will generally be uncertain. Examples:—

Let it be required to find (log sec) $^{-1}$ 0.0643; i.e. the angle of which the log sec is 0.0643. The nearest tabulated log sec is 0.0647. We have, then,

(log sec)⁻¹ 0.0647 = 30° 30′,
$$u_2 - u = 4$$
, $\Delta u = 7$, $\frac{4}{7} = 0.6$,
 \therefore (log sec)⁻¹ 0.0643 = 30° 30′ - 06′ = 30° 24′.

In like manner, let the student find

The angle may also be found by the next following table.

g. Pp. 8 and 9 may also be used for angles less than 6° or greater than 84°.

E.g.
$$l \sin 4^{\circ} 03'.4 = 8.8497$$
, $l \tan 4^{\circ} 03'.4 = 8.8508$, $l \sec 4^{\circ} 03'.4 = 0.0011$, $l \csc 4^{\circ} 03'.4 = 1.1503$, $l \cot 4^{\circ} 03'.4 = 1.1492$, $l \cos 4^{\circ} 03'.4 = 9.9989$.

§ 8. INVERSE CIRCULAR FUNCTIONS.

a. The table having this heading (pp. 16-18) is a table for finding the angle which corresponds to the given logarithm of a circular function. The logarithm (increased by 10) is the argument of the table, and is to be regarded as given to four places of decimals. It is tabulated at intervals of 0.0100 from 9.0000 to 0.0000 through the first page of the table, then at intervals of 0.0010, and in the last two divisions at intervals of 0.0001. characteristic of the argument is printed at the head of the column. figures supposed to follow the printed figures in the values of the argument Thus, the first value is 9.0000, the next 9.0100, etc. The angle is given, for convenience of interpolation, in degrees and decimals of a degree. When found, it is easily reduced to degrees and minutes, if that is necessary, and should, in general, be taken only to the nearest minute. angle under the heading $\sin^{-1} u$ is that angle of which the corresponding value of the argument, $\log u$, is the $\log \sin$; etc. In interpolating in this table, we may use the printed rate of difference instead of Δu , working from the nearest tabulated value of the argument, and carefully observing whether the tabulated angle ought to be increased or diminished. When the printed rate of difference is omitted, this is because the interval is too great to admit In this case, we must resort to those later of accurate interpolation. divisions of the table in which the argument is tabulated at smaller inter-When the last figure of the tabulated anyle is printed in small type, this shows that that figure is uncertain, if the logarithm is given to only four places; that is, that there is a possible variation, on each side of the tabulated angle, as great as half a unit in the place of the figure so printed. For example, if $\log u = 9.9000$, we find the last figures of $\sin^{-1} u$ and $\cos^{-1} u$ to be printed in small type. Now, seven-place tables show that (log sin)-1 $9.8999500 = 52^{\circ}.581$, while $(\log \sin)^{-1} 9.9000500 = 52^{\circ}.600$. But 9.9000 may represent any logarithm between these; and hence the corresponding angle, in this case, admits a like variation, while cos-1 u may have any value between 37°.419 and 37°.400.

Hyperbolic Functions.

Neither of these difficulties presents itself in finding an angle from its log tan or log ctn. If $\log u = 9.9000$, $\tan^{-1} u$ can only vary from 38°.458 to 38°.464.

The angle found by interpolation should be carried out only to the nearest hundredth of a degree, in any case. The last column of the table shows that the angle is not always determined even to the nearest tenth.

- b. If the characteristic of the given logarithm is 0, we must take its arithmetical complement, which will be the logarithm of the reciprocal function of the same angle. The angle can then be found by the table.
- c. If the given logarithm is less than 9.0000, or greater than 0.0000, the tables in the upper part of p. 10 may be used, as explained in \S 7, e; or pp. 8, 9.
- d. Let us find by this table the angles sought above, in § 7, f. We have, in the case of the first example,

$$(\log \sec)^{-1} 0.0643 = (\log \cos)^{-1} 9.9357.$$

Then the table gives

(log cos)⁻¹ 9.9360 = 30°.35,
$$\Delta u = 23$$
,
0.3 × 0.23 = .07
∴ (log cos)⁻¹ 9.9357 = 30°.42 = 30° 25′.

In fact, the limits of the angle are 30° 24'.2 and 30° 25'.6, the mean value being 30° 24'.9. In this case, the present table gives a better value than the other; but both values are admissible.

In like manner, we have

$$\begin{array}{l} (\log \sin)^{-1} \ 9.5663 = 21^{\circ}.81 - 20 = 21^{\circ}.61 = 21^{\circ} \ 37', \\ (\log \cos)^{-1} \ 9.9188 = 33^{\circ}.92 + .04 = 33^{\circ}.96 = 33^{\circ} \ 58', \\ (\log \tan)^{-1} \ 0.7507 = 79^{\circ}.92 + .02 = 79^{\circ}.94 = 79^{\circ} \ 56', \\ (\log \cot)^{-1} \ 0.0496 = 41^{\circ}.71 + .03 = 41^{\circ}.74 = 41^{\circ} \ 44', \\ (\log \sec)^{-1} \ 0.2272 = 53^{\circ}.64 + .02 = 53^{\circ}.66 = 53^{\circ} \ 40', \\ (\log \csc)^{-1} \ 0.1433 = 46^{\circ}.01 - .04 = 45^{\circ}.97 = 45^{\circ} \ 58'. \\ \end{array}$$

§ 9. HYPERBOLIC FUNCTIONS.

a. The hyperbolic functions are certain functions which bear relations to the equilateral hyperbola similar to those borne by the circular functions to the circle; and they may often be usefully employed both in computation and in analysis. They are named the hyperbolic sine, cosine, tangent, cotangent, secant, and cosecant; and are variously denoted by different writers. They are here represented by the symbols: Sh, Ch, Th, Cth, Sch, Csch. They may be defined by the following formulas, in which

$$G = \text{the exponential base}$$

$$= 1 + \frac{1}{1} + \frac{1}{1.2} + \frac{1}{1.2.3} + \frac{1}{1.2.3.4} + \dots$$

$$= 2.7182818285 \cdot \dots : -$$

$$Sh x = \frac{1}{4} (G^x - G^{-x}), \qquad Ch x = \frac{1}{4} (G^x + G^{-x}), \qquad Th x = \frac{Sh x}{Ch x},$$

$$Cth x = \frac{1}{Th x}, \qquad Sch x = \frac{1}{Ch x}, \qquad Csch x = \frac{1}{Sh x}$$

They bear to the circular functions the relations expressed by the following formulas, in which $i = \sqrt{-1}$:—

$$\operatorname{Sh} x = \frac{\sin xi}{i}, \qquad \qquad \sin x = \frac{\operatorname{Sh} xi}{i},$$

$$\operatorname{Ch} x = \cos xi, \qquad \qquad \cos x = \operatorname{Ch} xi,$$

$$\operatorname{Th} x = \frac{\tan xi}{i}, \qquad \qquad \tan x = \frac{\operatorname{Th} xi}{i},$$

$$\operatorname{Cth} x = i \operatorname{ctn} xi, \qquad \qquad \operatorname{ctn} x = i \operatorname{Cth} xi,$$

$$\operatorname{Sch} x = \sec xi, \qquad \qquad \operatorname{sec} x = \operatorname{Sch} xi,$$

$$\operatorname{Csch} x = i \operatorname{csc} xi, \qquad \operatorname{csc} x = i \operatorname{Csch} xi.$$

Again, if ϕ is so taken that

$$x= ant \log an (45^{\circ}+rac{1}{2}\phi),$$

$$\mathrm{Sh}\ x= an\ \phi,\qquad \mathrm{Ch}\ x=\sec\phi,\qquad \mathrm{Csch}\ x=\mathrm{ctn}\ \phi,$$

$$\mathrm{Th}\ x=\sin\phi,\qquad \mathrm{Sch}\ x=\cos\phi,\qquad \mathrm{Cth}\ x=\csc\phi.$$

The value of ϕ determined by this formula has been called by some writers the Gudermannian of x, and denoted by the symbol: gd x.

- b. From x=0.00 to x=1.00, the function tabulated is gd x in degrees, at intervals of 0.01 in the value of x. The hyperbolic functions of x are then readily found, by the aid of the formulas last given, from the tables of circular functions. Beginning with x=100, log Sh x, log Ch x, and log Th x are tabulated, at intervals of 0.01 in the value of x, up to x=3.00, the characteristic of each logarithm being placed at the head of its column; then at intervals of 0.1 up to x=6.0; and lastly at intervals of 1 up to x=10.0. The printed differences are to be used, as in other tables, each through half the interval before and after the line on which it stands.
- c. If x > 10, log Th x = 0.0000, while log Sh x and log Ch x may be found by the formula and table given at the lower right-hand corner of p. 21. The quantity μ is the modulus of the denary system of logarithms; that is, it is the denary logarithm of the exponential base. The values of $n \mu$ being given for all integral values of n from 1 to 10, any product $n \mu$ is readily found, by adding together the products of $n \mu$ by the successive figures of $n \mu$. Only four decimal-figures should be retained in the result.
- d. The functions $\log \operatorname{Cth} x$, $\log \operatorname{Sch} x$, and $\log \operatorname{Csch} x$ are the arithmetical complements of $\log \operatorname{Th} x$, $\log \operatorname{Ch} x$, and $\log \operatorname{Sh} x$, respectively.
 - e. The table may be used both directly and inversely. Examples: -

```
= \log \tan 29^{\circ}.427 = 9.7513,
 log Sh 0.5378
 log Ch 1.5280
                       = 0.3825.
 log Cth 1.8240
                       = 0.0226
 log Sh 12.5913
                       = \log \text{ Ch } 12.5913 = 5.1673,
 (log Ch)-1 1.6000
                       = 4.377.
 (\log Sh)^{-1} 5.0000
                       = 12.206.
(\log Th)^{-1} 9.9012
                       = 1.089.
(\log Sch)^{-1} 9.5873 = 1.604,
(\log Csch)^{-1} 0.3924 = gd^{-1} (\log tan)^{-1} 9.6078
    = gd^{-1} 22^{\circ}.06 = 0.395.
```

Natural Logarithms.

§ 10. NATURAL LOGARITHMS.

a. The natural system of logarithms is that which is founded on the exponential base (see § 9). This number is defined as the limiting value to which the expression

$$(1+\epsilon)^{\frac{1}{\epsilon}}=\sqrt[\epsilon]{(1+\epsilon)}$$

approaches, as ϵ approaches 0. It is most frequently denoted by the letter ϵ ; but, as being one of the few peculiar constants of analysis, it is here represented by the symbol \odot , which may be read "base."

The following formulas are proved in treatises on the Differential Calculus:—

$$6 = 1 + \frac{1}{1} + \frac{1}{1.2} + \frac{1}{1.2.3} + \frac{1}{1.2.34} + \dots,$$

$$6^{x} = 1 + \frac{x}{1} + \frac{x^{2}}{1.2} + \frac{x^{3}}{1.2.3} + \frac{x^{4}}{1.2.34} + \dots,$$

$$\text{nat log } (1+x) = x - \frac{x^{2}}{2} + \frac{x^{3}}{2} - \frac{x^{4}}{4} + \frac{x^{5}}{5} - \dots;$$

the second formula being applicable to all values of x, but the last only

when x is numerically less than 1. If x is very small, then approximately

$$6^x = 1 + x$$
, nat $\log (1 + x) = x$, nat $\log (1 - x) = -x$.

We also have, in the natural system,

$$\log (a + h) = \log a + \log \left(1 + \frac{h}{a}\right) = \log a + \frac{h}{a} - \frac{h^2}{2a^2} + \frac{h^3}{3a^3} - \dots,$$

provided h is numerically less than a.

The rate of difference of \mathfrak{S}^x , for $\Delta x = 1$, is always \mathfrak{S}^x , and that of nat $\log x$ is $\frac{1}{x}$.

b. The numerical value of \odot or of any power of \odot can be computed, to any assigned number of decimal-places, by using a sufficient number of terms of the first two series given above. Thus, to find \odot to four decimal-places, we proceed as follows, observing that, if any term be divided by its number in the series, the next following term is obtained:—

- 1) 1.00000
- 2) 1.00000
- 3) 0.50000
- 4) 0.16667
- 5) 0.04167
- 6) 0.00833
- 7) 0.00139
- 8; 0.00020

They bear to the circular functions the relations expr formulas, in which $i = \sqrt{-1}$:—

$$Sh x = \frac{\sin xi}{i}, \qquad \sin x = \frac{\sin xi}{i},$$

$$Ch x = \cos xi, \qquad \cos x = \frac{\tan xi}{i}, \qquad \tan x = \frac{\sin x}{i},$$

$$Cth x = i \cot xi, \qquad \cot x = \frac{\sin x}{i}$$

$$Sch x = \sec xi, \qquad \sec x = \frac{\sin x}{i}$$

$$Csch x = i \csc xi, \qquad \csc x = \frac{\sin x}{i}$$

Again, if ϕ is so taken that

$$x = \text{nat log tan } (45^{\circ} + \frac{1}{2} \phi),$$

Sh
$$x = \tan \phi$$
, Ch $x = \sec \phi$, Ch $x = \sec \phi$, Sch $x = \cos \phi$,

The value of ϕ determined by this formula has been the Gudermannian of x, and denoted by the symbol

- b. From x=0.00 to x=1.00, the function tabulate at intervals of 0.01 in the value of x. The hyperboli then readily found, by the aid of the formulas last g of circular functions. Beginning with x=1.00, $\log 8$ $\log 7$ the x are tabulated, at intervals of 0.01 in the value of 0.00, the characteristic of each logarithm being placed column; then at intervals of 0.1 up to x=6.0; and last up to x=10.0. The printed differences are to be use each through half the interval before and after the line of
- c. If x > 10, log Th x = 0.0000, while log Sh x are found by the formula and table given at the lower rip. 21. The quantity μ is the modulus of the denary systhat is, it is the denary logarithm of the exponential ban μ being given for all integral values of n from 1 to 10 readily found, by adding together the products of μ figures of x. Only four decimal-figures should be retain-
- d. The functions log Cth x, log Sch x, and log Csch complements of log Th x, log Ch x, and log Sh x, respective
 - e. The table may be used both directly and inversely.

			15					20			
	1.3	1.4	1.5	1.6	1.7	1.8		2.0	1		
- ,,	2.6 3.9	2.8 4.2	3.0 4.5	3.2 4.8	3.4 5.1	3.6 5.4	3.8 5.7	4.0 6.0	3		
• • •		5.6	6.0	6.4	6.8	7.2	7.6	8.0	4		
	6.5	7.0	7.5	8.0	8.5	9.0		10.0	5		
	7.8	8.4	9.0		10.2				6		
	9.1	9.8	10.5		11.9 13.6				7 8		
		12.6			15.3				9		
-			35					40	_		
_	3. 3	3.4	3.5	3,6	3.7	3.8	3.9	4.0	1		
~ (6.6	6.8	7.0	7.2	7.4			8.0	2		
		10.2			11.1				3 4		
	13.2 16.5	13.6 17.0			14.8 18.5				5		
		20.4			22.2				6		
	23.1	23.8	24.5		25.9				7		
		27.2			29.6 33.3				8		
	29.7	30.6	31.5	32.4	33.3	34.2	30.1		اٿا		
			55					60			
	5 .3	5.4	5.5	5.6		5.8		6.0	1		
	10.6 15.9				11.4 17.1				3		
١, (21.6			22.8				4		
(26.5				28.5				5		
		32. 4			34.2				6		
	37.1				39.9 45.6			42.0 48.0	7 8		
	47.7	43.2 48.6			51.3				0		
_		20.0	75					80			
	7.3	7.4	7.5	7.6	7.7	7.8	7.9	8.0	1		
• 4	14.6			15.2	15.4				2		
	21.9				23.1				3		
	29.2				30.8 38.5				4 5		
	36.5 43.8				46.2				6		
	51.1			53.2	53.9	54.6	55.3	56.0	7		
	5 8.4				61.6				8		
	65.7	66.6	67.5	68.4	69.3	70.2	71.1	72.0	۳		
			95			100					
	9.3		9.5	9.6	9.7 19.4			10.0	1 2		
	18.6 27.9			28.8	19.4 29.1	29.4	29.7	30.0	3		
	37.2			38.4	38.8	39.2	39.6	40.0	4		
4.0	46.5	47.0	47.5	48.0	48.5	49.0	49.5	50.0	5		
	55.8			/ 27 5	י רם י	282	RA A	0.00 2018:	16		
			д.88. г.вг s	, / ne	0 77	8 41	r 4.6	8:5 R	1 0.0		
3. 2	8 83.	7 84	<i>₹8 θ.</i>	$g \mid \vec{\sigma}$	8.4.8	8.12	88.5	88:7	0.08		

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§ 2, c, and completely illustrated below, in the explanation of the table of Logarithms of Circular Functions. The table of Proportional Parts may be employed in computing the corrections. Examples:—

(3)
$$1.0960 = 1.1295$$
,
 (3) $(7.5265 - 10) = 0.0015$,

 (4) $3.8129 = 3.8130$,
 (5) $(9.6431 - 10) = 0.1582$.

 16 $\log x < 6.0000 - 10$,
 $\log (x + 1) = 0.0000$ to four places;

 16 $\log x > 4.0000$,
 $\log (x + 1) = \log x$ to four places.

c. To find the anti-Gaussian of a given logarithm. Seek, in the body of the table, two successive logarithms between which the given logarithm lies, and then find the corresponding value of the argument by interpolation. Examples:—

$$\mathfrak{G}^{-1}$$
 1.0960 = 1.0597, \mathfrak{G}^{-1} 0.1051 = 9.4373 — 10, \mathfrak{G}^{-1} 3.8129 = 3.8128, \mathfrak{G}^{-1} 1.0216 = 0.9782.

d. To find the logarithm of the sum or difference of the antilogarithms of two given logarithms. If m and n are two numbers,

$$m+n=n\left(\frac{m}{n}+1\right), \qquad m-n=n\left(\frac{m}{n}-1\right),$$

$$\log (m+n)=\log n+\log \left(\frac{m}{n}+1\right)=\log n+ \mathfrak{G}\log \frac{m}{n},$$

$$\log (m-n)=\log n+\log \left(\frac{m}{n}-1\right)=\log n+ \mathfrak{G}^{-1}\log \frac{m}{n}.$$

Example:—

Given
$$a=4.142$$
, $b=2.399$; to find $\sqrt{(a^2+b^2)}$ and $\sqrt{(a^2-b^2)}$.
log $a=0.6172$, log $b=0.3800$,
log $a^2=1.2344$, log $b^2=0.7600$,
log $\frac{a^2}{b^2}=0.4744$;
 $\Im \log \frac{a^2}{b^2}=0.6000$, $\Im \log \frac{a^2}{b^2}=0.2970$,
log $b^2=0.7600$, log $b^2=0.7600$,
log $(a^2+b^2)=1.3600$, log $(a^2-b^2)=1.0570$,
log $\sqrt{(a^2+b^2)}=0.6800$, $\sqrt{(a^2-b^2)}=0.5285$,
 $\sqrt{(a^2+b^2)}=4.787$; $\sqrt{(a^2-b^2)}=3.377$.

§ 6. CIRCULAR, OR TRIGONOMETRIC, FUNCTIONS: NATURAL VALUES.

a. Three tables of the natural values of the trigonometric functions are given on pp. 22-27. Each table is broken up into six divisions, and occupies two pages. The argument is the angle, which is tabulated at intervals of 10' from 0° to 90°. Angles in the first half of the quadrant will be found in the left-hand column of the several divisions of the table, and for those angles the names of the functions are to be taken from the top of the page; angles in the second half of the quadrant are to be found in the right-hand

Logarithms of Circular Functions.

column of the table, and for those angles the names of the functions are to be taken from the bottom of the page. The angles standing at the right and left in the same line are complements of each other; and the names of the functions at the top and bottom of the same column are complementary. The value of any of the functions for a non-tabulated angle, or the value of the angle for a non-tabulated value of one of the functions, can be found by the method of interpolation explained in § 2. The precepts of § 2, d, e, should be observed in computing the corrections. The tabulated values of the functions are generally given to four significant figures; but, in the tables of tangents and secants, they are sometimes given to a less number of figures (to avoid errors in interpolation), and are sometimes omitted altogether. In these cases the functions can be best found by finding their logarithms by the table of Logarithms of Circular Functions (see § 7), and then the numbers corresponding by the table of Logarithms.

- b. To find any function of an angle greater than 90°, we must subtract from the given angle the greatest multiple of 90° which it contains; if an even multiple has been subtracted, we look out the required function of the remainder; if an odd multiple, the complementary function; and we then fix the sign of the function by considering the quadrant in which the given angle lies. For a negative angle, we find the required function of the corresponding positive angle, and then fix its sign by considering the quadrant of the angle.
 - c. Examples of the use of these tables: —

```
sin 77° 37'
                        0.9767, tan 53^{\circ} 04' = 1.330,
                                                                     sec 68° 45' =
                                                                                            2.759.
cos 16º 19'
                        0.9597,
                                   ctn
                                           3° 18′ =
                                                           17.4,
                                                                    csc 55^{\circ} 13' =
                                                                                            1.217:
\sin 257^{\circ} 37' = -0.9767, \tan 93^{\circ} 18' = -17.4,
                                                                     sec 325° 13′ =
                                                                                            1.217,
\cos 163^{\circ} 41' = -0.9597, \cot 323^{\circ} 04' = -1.330, \csc 158^{\circ} 45' =
                                                                                            2.759;
\sin(-257^{\circ}37') = 0.9767, \tan(-93^{\circ}18') = 17.4, \sec(-325^{\circ}13') =
\cos(-163^{\circ}41') = -0.9597, \cot(-323^{\circ}04') = 1.330, \csc(-158^{\circ}45') = -2.759;
                                 11^{\circ} 32' \text{ or } = 168^{\circ} 28' \text{ or } =
     \sin^{2} 0.2000
                                                                           371° 32′, etc.,
                            =
     \cos^{-1}(-0.3542) = 110^{\circ} 45' \text{ or } = 249^{\circ} 15' \text{ or } = 830^{\circ} 45', \text{ etc.},
     tan^{-1} (-4.570) = 102° 21′ or = 282° 21′ or = -77° 39′, etc.,
                                  72^{\circ} \ 27' \text{ or } = 252^{\circ} \ 27' \text{ or } = -107^{\circ} \ 33', \text{ etc.},
     ctn-1 0.3163
                            =
                                  78^{\circ} \ 28' \text{ or } = -78^{\circ} \ 28' \text{ or } = \pm 281^{\circ} \ 32', \text{ etc.},
     sec-1 5.000
     csc^{-1} (-3.529) = -16° 28′ or = 196° 28′ or = -163° 32′, etc.
```

§ 7. LOGARITHMS OF CIRCULAR FUNCTIONS.

To find the logarithm of any circular function of a given angle.

a. If the angle is less than 6° , the part of the table which occupies the upper half of p. 10 may be used. (See also g.) The left-hand division of this part of the table gives the values of a logarithm S (the characteristic and the first two figures of the mantissa being printed at the head of the column), with the angular limits between which each value may be used. Thus, for all positive angles less than 1° 51'.479, S = 6.4637; for all angles between 1° 51'.479 and 2° 49'.567, S = 6.4638; etc. The next following

division gives, in like manner, the values of a logarithm T. We must find the logarithm of the angle, reduced to minutes and decimals of a minute, and must then apply the formulas:—

```
\log \sin \phi = \log (\phi \text{ in minutes}) + S - 10,

\log \tan \phi = \log (\phi \text{ in minutes}) + T - 10.
```

The two right-hand divisions of this part of the table give the values of the log sec, with the angular limits for each value. The logarithms of the cosine, cotangent, and cosecant are the arithmetical complements (— 10) of the logarithms of the secant, tangent, and sine, respectively. Example:—

```
l sin 3° 15′.23 = 8.7541, l tan 3° 15′.23 = 8.7548, l sec 3° 15′.23 = 0.0007, l csc 3° 15′.23 = 1.2459, l ctn 3° 15′.23 = 1.2452, l cos 3° 15′.23 = 9.9993;
```

the negative characteristics being here, as in the following examples, made positive by the addition of 10.

b. If the angle is acute and greater than 84°, we must take its complement, and then seek the function complementary to that required, for the angle thus obtained, by the method just expounded. Example:—

```
l sin 86° 44′.77 = 9.9993, l tan 86° 44′.77 = 1.2452, l sec 86° 44′.77 = 1.2459, l csc 86° 44′.77 = 0.0007, l ctn 86° 44′.77 = 8.7548, l cos 86° 44′.77 = 8.7541.
```

c. If the angle is contained between 6° and 84°, we use the main part of the table, occupying the lower half of p. 10 and pp. 11-15. The angle is tabulated at intervals of 10', from 6° to 45° in the left-hand column of the table. and from 45° to 84° in the right-hand column. The names of the functions are to be taken from the tops of the columns, when the angle is on the left; and from the bottoms of the columns, when the angle is on the right. The angles on the right and left of any line and the names at the top and bottom of any column have the same relation to each other as in the tables of Natural Values (§ 6). The true characteristic in the first, third, and sixth columns is -1, but is printed 9. The six columns are arranged in pairs. The two functions in each pair of columns are reciprocal to each other; and the logarithms are therefore complementary, and their differences are equal in value, with opposite signs. Down the middle of each double column are printed, in small type, the rates of difference of the logarithms in that double column. Each value of this rate may be used in interpolation, instead of Δu , through half the interval before and after the line on which it stands, as stated in § 2, c. Thus, in finding the logarithms of the circular functions of any angle between 25° 25' and 25° 35' we work from the values corresponding to 25° 30', the nearest tabulated angle; and compute the corrections by taking proportional parts of 26, 33, and 6, for the three pairs of functions. In applying the corrections, we must carefully observe, for each function, whether the function is increasing or decreasing.

For example, let the logarithms of the circular functions of 25° 27'.4 = 25° 30' — 02'.6 be required. We find

```
    1 \sin 25^{\circ} 30' = 9.6340
    1 \tan 25^{\circ} 30' = 9.6785
    1 \sec 25^{\circ} 30' = 0.0445

    0.26 \times 26 = 7
    0.26 \times 33 = 9
    0.26 \times 6 = 2

    1 \sin 25^{\circ} 27'.4 = 9.6333
    1 \tan 25^{\circ} 27'.4 = 9.6776
    1 \sec 25^{\circ} 27'.4 = 0.0445
```

Logarithms of Circular Functions.

In like manner, we have

$$1 \sin 74^{\circ} 46' = 9.9845$$
, $1 \tan 74^{\circ} 46' = 0.5849$, $1 \sec 74^{\circ} 46' = 0.5804$, $1 \csc 74^{\circ} 46' = 0.0155$, $1 \cot 74^{\circ} 46' = 9.4351$, $1 \cos 74^{\circ} 46' = 9.4196$.

d. If the angle is greater than 90° , or negative, we must use the method explained in § 6, b, for the tables of Natural Values of the circular functions. When the natural value of a circular function is negative, this should be indicated by writing the letter n after its logarithm. Examples:

```
l sin 105° 14′ = 9.9845, l tan 105° 14′ = 0.5649 n, l sec 105° 14′ = 0.5804 n, l csc 164° 46′ = 0.5804, l ctn 164° 46′ = 0.5649 n, l cos 164° 46′ = 9.9845 n, l sin (-74° 46′) = 9.9845 n, l tan (-105° 14′) = 0.5649, l cos (-394° 46′) = 9.4196.
```

Given the logarithm of any circular function, to find the value of the corresponding angle.

e. If the given logarithm lies without the limits of the main part of the table, the upper part of p. 10 may be used. If the given logarithm is a log sin less than 9.0192, or a log tan less than 9.0216, subtract from it the proper value of S or T (or add the arithmetical complement), and the remainder is the log of the required angle in minutes. The limiting values of the log sin and log tan for each value of S and T are given in the table. If the given log is a log csc greater than 0.9808, or a log ctn greater than 0.9784, its arithmetical complement will be a log sin less than 9.0192, or a log tan less than 9.0216. If the given log is a log sec less than 0.0024, the limits between which the required angle lies are given by the table; the angle may have any value between these limits, and is not therefore very closely determined. If the given log is a log cos greater than 9.9976, its arithmetical complement is a log sec less than 0.0024.

If the given log is a log sin, log tan, or log sec greater than 9.9976, 0.9784, or 0.9808 (respectively), or a log csc, log ctn, or log cos less than 0.0024, 9.0216, or 9.0192 (respectively), we must change the name of the function to the complementary name (sin to cos, etc.), find the corresponding angle as above, and take the complement of the angle thus found. Examples:—

$$(\log \sin)^{-1} 8.9542 = 5^{\circ} 09'.8,$$
 $(\log \cot)^{-1} 2.0531 = 0^{\circ} 30'.42,$ $(\log \cot)^{-1} 9.0024 = 84^{\circ} 15'.5,$ $(\log \sin)^{-1} 9.9983 = 84^{\circ} 56' \pm 4\frac{1}{2}'.$

f. If the given logarithm is contained within the limits of the main part of the tuble, the required angle is found by ordinary interpolation; and we may use the printed rate of difference as the value of Δu , working in each case from the nearest tabulated value. The angle should be found to the nearest minute, or, when the difference exceeds 100, to the nearest lends of a

minute. But in the right-hand pair of columns, the last figure of the angle thus found will generally be uncertain. Examples: -

Let it be required to find (log sec)-1 0.0343; i.e. the angle of which the log sec is 0.0643. The nearest tabulated log sec is 0.0647. We have, then,

(log sec)⁻¹ 0.0647 = 30° 30′,
$$u_2 - u = 4$$
, $\Delta u = 7$, $\frac{4}{7} = 0.6$,
 \therefore (log sec)⁻¹ 0.0643 = 80° 30′ - 06′ = 30° 24′.

In like manner, let the student find

$$(\log \sin)^{-1} 9.5663 = 21^{\circ} 37',$$
 $(\log \cos)^{-1} 9.9188 = 33^{\circ} 58' \text{ or } 57',$ $(\log \sec)^{-1} 0.2272 = 53^{\circ} 39',$ $(\log \tan)^{-1} 0.7507 = 79^{\circ} 56',$ $(\log \csc)^{-1} 0.1433 = 45^{\circ} 58'.$

The angle may also be found by the next following table.

q. Pp. 8 and 9 may also be used for angles less than 6° or greater than 84°.

E.g.
$$1 \sin 4^{\circ} 03'.4 = 8.8497$$
, $1 \tan 4^{\circ} 03'.4 = 8.8508$, $1 \sec 4^{\circ} 03'.4 = 0.0011$, $1 \csc 4^{\circ} 03'.4 = 1.1503$, $1 \cot 4^{\circ} 03'.4 = 1.1492$, $1 \cos 4^{\circ} 03'.4 = 9.9989$.

§ 8. INVERSE CIRCULAR FUNCTIONS.

a. The table having this heading (pp. 16-18) is a table for finding the angle which corresponds to the given logarithm of a circular function. logarithm (increased by 10) is the argument of the table, and is to be regarded as given to four places of decimals. It is tabulated at intervals of 0.0100 from 9.0000 to 0.0000 through the first page of the table, then at intervals of 0.0010, and in the last two divisions at intervals of 0.0001. characteristic of the argument is printed at the head of the column. figures supposed to follow the printed figures in the values of the argument Thus, the first value is 9.0000, the next 9.0100, etc. The angle is given, for convenience of interpolation, in degrees and decimals of a degree. When found, it is easily reduced to degrees and minutes, if that is necessary, and should, in general, be taken only to the nearest minute. The angle under the heading $\sin^{-1} u$ is that angle of which the corresponding value of the argument, log u, is the log sin; etc. In interpolating in this table, we may use the printed rate of difference instead of Δu , working from the nearest tabulated value of the argument, and carefully observing whether the tabulated angle ought to be increased or diminished. When the printed rate of difference is omitted, this is because the interval is too great to admit In this case, we must resort to those later of accurate interpolation. divisions of the table in which the argument is tabulated at smaller inter-When the last figure of the tabulated angle is printed in small type, this shows that that figure is uncertain, if the logarithm is given to only four places; that is, that there is a possible variation, on each side of the tabulated angle, as great as half a unit in the place of the figure so printed. For example, if $\log u = 9.9000$, we find the last figures of $\sin^{-1} u$ and $\cos^{-1} u$ to be printed in small type. Now, seven-place tables show that (log sin)-1 $9.8999500 = 52^{\circ}.581$, while $(\log \sin)^{-1} 9.9000500 = 52^{\circ}.600$. But 9.9000may represent any logarithm between these; and hence the corresponding

angle, in this case, admits a like variation, while cos-1 u may have any *value between 37°.419* and 37°.400.

Hyperbolic Functions.

Neither of these difficulties presents itself in finding an angle from its log tan or log ctn. If $\log u = 9.9000$, $\tan^{-1} u$ can only vary from 38°.458 to 38°.464.

The angle found by interpolation should be carried out only to the nearest hundredth of a degree, in any case. The last column of the table shows that the angle is not always determined even to the nearest tenth.

- b. If the characteristic of the given logarithm is 0, we must take its arithmetical complement, which will be the logarithm of the reciprocal function of the same angle. The angle can then be found by the table.
- c. If the given logarithm is less than 9.0000, or greater than 0.0000, the tables in the upper part of p. 10 may be used, as explained in \S 7, e; or pp. 8, 9.
- d. Let us find by this table the angles sought above, in § 7, f. We have, in the case of the first example,

$$(\log \sec)^{-1} 0.0643 = (\log \cos)^{-1} 9.9357.$$

Then the table gives

(log cos)⁻¹ 9.9360 = 30°.35,
$$\Delta u = 23$$
,
0.3 × 0.23 = .07
∴ (log cos)⁻¹ 9.9357 = 30°.42 = 30°.25′.

In fact, the limits of the angle are 30° 24'.2 and 30° 25'.6, the mean value being 30° 24'.9. In this case, the present table gives a better value than the other; but both values are admissible.

In like manner, we have

§ 9. HYPERBOLIC FUNCTIONS.

a. The hyperbolic functions are certain functions which bear relations to the equilateral hyperbola similar to those borne by the circular functions to the circle; and they may often be usefully employed both in computation and in analysis. They are named the hyperbolic sine, cosine, tangent, cotangent, secant, and cosecant; and are variously denoted by different writers. They are here represented by the symbols: Sh, Ch, Th, Cth, Sch, Csch. They may be defined by the following formulas, in which

$$G = \text{the exponential base}$$

$$= 1 + \frac{1}{1} + \frac{1}{1.2} + \frac{1}{1.2.3} + \frac{1}{1.2.3.4} + \dots$$

$$= 2.7182818285 \cdot \dots : -$$

$$\text{Sh } x = \frac{1}{4} (G^x - G^{-x}), \qquad \text{Ch } x = \frac{1}{4} (G^x + G^{-x}), \qquad \text{Th } x = \frac{\text{Sh } x}{\text{Ch } x},$$

$$Cth x = \frac{1}{Th x}, \qquad \text{Sch } x = \frac{1}{Ch x}, \qquad Cech x = \frac{1}{Sh x}$$

They bear to the circular functions the relations expressed by the following formulas, in which $i = \sqrt{-1}$:—

$$\operatorname{Sh} x = \frac{\sin xi}{i}, \qquad \sin x = \frac{\operatorname{Sh} xi}{i},$$

$$\operatorname{Ch} x = \cos xi, \qquad \cos x = \operatorname{Ch} xi,$$

$$\operatorname{Th} x = \frac{\tan xi}{i}, \qquad \tan x = \frac{\operatorname{Th} xi}{i},$$

$$\operatorname{Cth} x = i \operatorname{ctn} xi, \qquad \cot x = i \operatorname{Cth} xi,$$

$$\operatorname{Sch} x = \sec xi, \qquad \sec x = \operatorname{Sch} xi,$$

$$\operatorname{Csch} x = i \operatorname{csc} xi, \qquad \csc x = i \operatorname{Csch} xi.$$

Again, if ϕ is so taken that

$$x=$$
 nat log tan $(45^{\circ}+\frac{1}{4}\phi)$,
Sh $x=$ tan ϕ , Ch $x=$ sec ϕ , Csch $x=$ ctn ϕ ,
Th $x=$ sin ϕ , Sch $x=$ cos ϕ , Cth $x=$ csc ϕ .

The value of ϕ determined by this formula has been called by some writers the Gudermannian of x, and denoted by the symbol: gd x.

- b. From x=0.00 to x=1.00, the function tabulated is gd x in degrees, at intervals of 0.01 in the value of x. The hyperbolic functions of x are then readily found, by the aid of the formulas last given, from the tables of circular functions. Beginning with x=1.00, log Sh x, log Ch x, and log Th x are tabulated, at intervals of 0.01 in the value of x, up to x=3.00, the characteristic of each logarithm being placed at the head of its column; then at intervals of 0.1 up to x=6.0; and lastly at intervals of 1 up to x=10.0. The printed differences are to be used, as in other tables, each through half the interval before and after the line on which it stands.
- c. If x > 10, log Th x = 0.0000, while log Sh x and log Ch x may be found by the formula and table given at the lower right-hand corner of p. 21. The quantity μ is the modulus of the denary system of logarithms; that is, it is the denary logarithm of the exponential base. The values of $n \mu$ being given for all integral values of n from 1 to 10, any product $n \mu$ is readily found, by adding together the products of $n \mu$ by the successive figures of $n \mu$. Only four decimal-figures should be retained in the result.
- d. The functions $\log \operatorname{Cth} x$, $\log \operatorname{Sch} x$, and $\log \operatorname{Csch} x$ are the arithmetical complements of $\log \operatorname{Th} x$, $\log \operatorname{Ch} x$, and $\log \operatorname{Sh} x$, respectively.
 - e. The table may be used both directly and inversely. Examples: -

```
= \log \tan 29^{\circ}.427 = 9.7513,
 log Sh 0.5378
 log Ch 1.5280
                         = 0.3825
 log Cth 1.8240
                         = 0.0226,
 log Sh 12.5913
                         = \log \text{Ch } 12.5913 = 5.1673,
 (log Ch)-1 1.6000
                         = 4.377,
 (\log Sh)^{-1} 5.0000
                         = 12.206
 (\log Th)^{-1} 9.9012
                        = 1.089
(\log Sch)^{-1} 9.5873 = 1.604,
(\log \operatorname{Csch})^{-1} 0.3924 = \operatorname{gd}^{-1} (\log \tan)^{-1} 9.6076
     = gd^{-1} 22^{\circ}.06 = 0.395.
```

Natural Logarithms.

§ 10. NATURAL LOGARITHMS.

a. The natural system of logarithms is that which is founded on the exponential base (see § 9). This number is defined as the limiting value to which the expression

$$(1+\epsilon)^{\frac{1}{\epsilon}}=\sqrt[6]{(1+\epsilon)}$$

approaches, as e approaches 0. It is most frequently denoted by the letter e; but, as being one of the few peculiar constants of analysis, it is here represented by the symbol 6, which may be read "base."

The following formulas are proved in treatises on the Differential Calculus:—

$$G = 1 + \frac{1}{1} + \frac{1}{1.2} + \frac{1}{1.2.3} + \frac{1}{1.2.3.4} + \dots,$$

$$G^{x} = 1 + \frac{x}{1} + \frac{x^{2}}{1.2} + \frac{x^{3}}{1.2.3} + \frac{x^{4}}{1.2.3.4} + \dots,$$

$$\operatorname{nat log}(1+x) = x - \frac{x^{2}}{2} + \frac{x^{3}}{3} - \frac{x^{4}}{4} + \frac{x^{6}}{5} - \dots;$$

the second formula being applicable to all values of x, but the last only when x is numerically less than 1. If x is very small, then approximately

$$6^{x} = 1 + x$$
, nat $\log (1 + x) = x$, nat $\log (1 - x) = -x$.

We also have, in the natural system,

$$\log (a + h) = \log a + \log \left(1 + \frac{h}{a}\right) = \log a + \frac{h}{a} - \frac{h^2}{2a^2} + \frac{h^3}{3a^3} - \dots,$$
 provided h is numerically less than a.

The rate of difference of G^x , for $\Delta x = 1$, is always G^x , and that of nat $\log x$ is $\frac{1}{x}$.

b. The numerical value of \odot or of any power of \odot can be computed, to any assigned number of decimal-places, by using a sufficient number of terms of the first two series given above. Thus, to find \odot to four decimal-places, we proceed as follows, observing that, if any term be divided by its number in the series, the next following term is obtained:—

- 1) 1.00000
- 2) 1.00000
- 3) 0.50000
- 4) 0.16667
- 5) 0.04167
- 6) 0.00833
- 7) 0.00139
- 8) 0.00020 0.00002
- $G = 2.7183 \dots$

c. The modulus of any system of logarithms is the logarithm of G in that system. If m is the modulus of a system of which a is the base, then

$$a^{m} = 6, \qquad 6^{m-1} = a.$$

The modulus of the natural system itself is 1. The values of the modulus of the denary system and of the reciprocal of that modulus are

$$\mu$$
 = den log \odot = 0.4342944819...,
 μ^{-1} = nat log 10 = 2.3025850930....

By the rule for converting logarithms from one system to another, the logarithm of a number in any system may be found by multiplying the modulus of that system into the natural logarithm of the same number. Thus,

den
$$\log x = \mu$$
 nat $\log x$,
nat $\log x = \mu^{-1}$ den $\log x$.

By the aid of these formulas, the table at the bottom of p. 21 may be used to find the natural logarithm of any number, or the denary logarithm of any power of the exponential base, or to find a number from its natural logarithm. For example:—

nat log 72.5 =
$$1.8603 \times \mu^{-1} = 4.2835$$
,
nat log $1.0074 = 0.0032 \times \mu^{-1} = 0.0074$,
den log $6^{\frac{1}{7}} = \frac{1}{7}\mu = 0.0620$,
(nat log)⁻¹ $10.2108 = (\text{den log})^{-1} (10.2108 \times \mu)$
= $(\text{den log})^{-1} 4.4345 = 27194$.

- d. The natural system is so called, because, in the higher mathematics, it is convenient to regard all other systems as founded upon this. It is named by some writers hyperbolic, and by others Neperian. But in fact, it is not the system of Napier; nor has it any other relation to the hyperbola than that which belongs to logarithms in general.
- e. We may make the following statement of the relation of logarithms and of the hyperbolic functions to the hyperbola, using the notation of Analytic Geometry:—

Let xy=1 be the equation of an hyperbola referred to its asymptotes. It can be proved by the Integral Calculus that the area, contained between the curve and the axis of x, and between two ordinates of which one is drawn to the vertex of the curve, is measured by $\log x$ in the system of which the modulus is $\sin \omega$. Thus, the logarithms belonging to any system may be represented by the areas of an appropriate hyperbola. The natural system corresponds to the equilateral hyperbola, for which $\sin \omega = 1$.

Again, if u denotes twice the area of the sector of the hyperbola $x^2 - y^2 = 1$, contained between the axis of x and a radius vector from the centre, then

$$x = \operatorname{Ch} u, \qquad y = \operatorname{Sh} u;$$

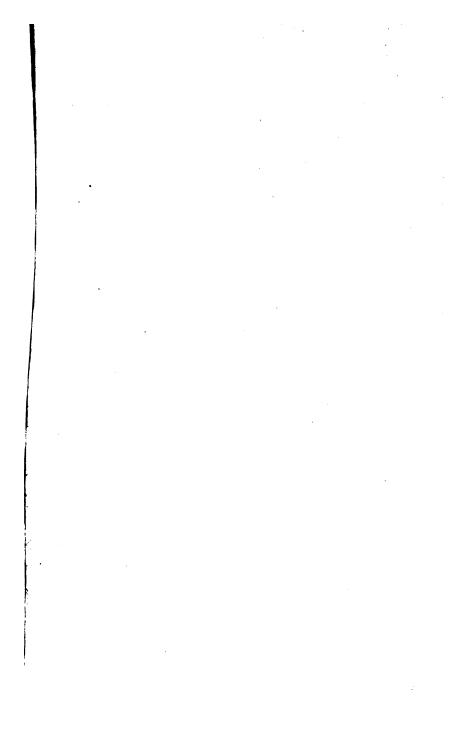
fust as, in the circle $x^2 + y^2 = 1$, with a similar meaning of u,

$$x = \cos u$$
. $y = \sin u$.

Proportional Parts.

		10					15					20	
0.8	0.9	1.0	1.1	1.2	1.3	1,4	1.5	1.6	1.7	1.8	1.9	2.0	l i
1.6		2.0	2.2	2.4	2.6	2.8	3.0	3.2	3.4	3.6	3.8	4.0	2
2.4		3.0	3.3	3.6	3.9	4.2	4.5	4.8	5.1	5.4	5.7	6.0	3
3.2	3.6	4.0	4.4	4.8	5.2	5.6	6.0	6.4	6.8	7.2	7.6	8.0	4
4.0	4.5	5.0	5.5	6,0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	5
4.8	5.4	6.0	6.6	7.2	7.8	8.4	9.0	9.6	10.2	10.8	11.4	12.0	6
5. 6	6.3	7.0	7.7	8.4	9.1		10.5	11.2					7
6.4	7.2	8.0	8.8		10.4			12.8					8
7.2 8.1 9.0 9.9 10.8 11.7 12.6 13.5 14.4 15.3 16.2 17.1 18.0 9										9			
30							35					40	
2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3,6	3.7	3.8	3.9	4.0	1
5. 6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4		7.8		2
8.4		9.0	9.3	9.6		10.2				11.4			3
	11.6			12.8						15.2			4
	14.5			16.0				18.0					5
	17.4			19.2				1		22.8			6
	20.3			22.4				25.2 28.8					7 8
	23.2 26.1			25.6 28.8				32.4					9
J. A	20.1		21.0	20.0	2011	00.0		02.12	00.0				Ľ
		50					55	50	5.77	5.0	5.0	6.0	<u> </u>
4.8	4.9	5.0	5.1	5.2	5.3	5.4		5.6 11.2	5.7	5.8	5.9		1 2
9.6	14.7	10.0		10.4 15.6				16.8					3
	19.6			20.8				22.4					4
	24.5			26.0				28.0					6
	29.4			31.2				33.6					6
	34.3			36.4				39.2	39.9	40.6	41.3	42.0	7
	39.2			41.6				44.8	45.6	46.4	47.2	48.0	8
	44.1			46.8				50.4	51.3	52.2	53.1	54.0	9
		70					75					80	
6.8	6.9	7.0	7.1	7.2	7.3	7.4	7.5					1	
						, , <u>, , , , , , , , , , , , , , , , , </u>	,,,,	7.6	7.7	7.8	7.9	8.0	1
		14.0	14.2	14,4	14.6	14.8	15.0	15.2	15.4	15.6	15.8	16.0	2
0.4	20.7	21.0	14.2 21.3	21.6	14.6 21.9	14.8 22.2	15.0 22.5	15.2 22.8	15.4 23.1	15.6 23.4	15.8 23.7	16.0 24.0	2 3
0.4 7.2	20.7 27.6	21.0 28.0	14.2 21.3 28.4	21.6 28.8	14.6 21.9 29.2	14.8 22.2 29.6	15.0 22.5 30.0	15.2 22.8 30.4	15.4 23.1 30.8	15.6 23.4 31.2	15.8 23.7 31.6	16.0 24.0 32.0	2 3 4
0.4 7.2 4.0	20.7 27.6 34.5	21.0 28.0 35.0	14.2 21.3 28.4 35.5	21.6 28.8 36.0	14.6 21.9 29.2 36.5	14.8 22.2 29.6 37.0	15.0 22.5 30.0 37.5	15.2 22.8 30.4 38.0	15.4 23.1 30.8 38.5	15.6 23.4 31.2 39.0	15.8 23.7 31.6 39.5	16.0 24.0 32.0 40.0	2 3 4 5
0.4 7.2 4.0 0.8	20.7 27.6 34.5 41.4	21.0 28.0 35.0 42.0	14.2 21.3 28.4 35.5 42.6	21.6 28.8 36.0 43.2	14.6 21.9 29.2 36.5 43.8	14.8 22.2 29.6 37.0 44.4	15.0 22.5 30.0 37.5 45.0	15.2 22.8 30.4 38.0 45.6	15.4 23.1 30.8 38.5 46.2	15.6 23.4 31.2 39.0 46.8	15.8 23.7 31.6 39.5 47.4	16.0 24.0 32.0 40.0 48.0	2 3 4 5 6
0.4 7.2 4.0 0.8 7.6	20.7 27.6 34.5 41.4 48.3	21.0 28.0 35.0 42.0 49.0	14.2 21.3 28.4 35.5 42.6 49.7	21.6 28.8 36.0 43.2 50.4	14.6 21.9 29.2 36.5 43.8 51.1	14.8 22.2 29.6 37.0 44.4 51.8	15.0 22.5 30.0 37.5 45.0 52.5	15.2 22.8 30.4 38.0 45.6 53.2	15.4 23.1 30.8 38.5 46.2 53.9	15.6 23.4 31.2 39.0 46.8 54.6	15.8 23.7 31.6 39.5 47.4 55.3	16.0 24.0 32.0 40.0 48.0 56.0	2 3 4 5 6 7
0.4 7.2 4.0 0.8 7.6 4.4	20.7 27.6 34.5 41.4 48.3 55.2	21.0 28.0 35.0 42.0 49.0 56.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8	21.6 28.8 36.0 43.2 50.4 57.6	14.6 21.9 29.2 36.5 43.8 51.1 58.4	14.8 22.2 29.6 37.0 44.4 51.8 59.2	15.0 22.5 30.0 37.5 45.0 52.5 60.0	15.2 22.8 30.4 38.0 45.6 53.2 60.8	15.4 23.1 30.8 38.5 46.2 53.9 61.6	15.6 23.4 31.2 39.0 46.8 54.6 62.4	15.8 23.7 31.6 39.5 47.4 55.3 63.2	16.0 24.0 32.0 40.0 48.0 56.0 64.0	2 3 4 5 6
0.4 7.2 4.0 0.8 7.6 4.4	20.7 27.6 34.5 41.4 48.3	21.0 28.0 35.0 42.0 49.0 56.0 63.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8	21.6 28.8 36.0 43.2 50.4	14.6 21.9 29.2 36.5 43.8 51.1 58.4	14.8 22.2 29.6 37.0 44.4 51.8 59.2	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5	15.2 22.8 30.4 38.0 45.6 53.2	15.4 23.1 30.8 38.5 46.2 53.9 61.6	15.6 23.4 31.2 39.0 46.8 54.6 62.4	15.8 23.7 31.6 39.5 47.4 55.3 63.2	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0	2 3 4 5 6 7 8
0.4 7.2 4.0 0.8 7.6 4.4 1.2	20.7 27.6 34.5 41.4 48.3 55.2 62.1	21.0 28.0 35.0 42.0 49.0 56.0 63.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8 63.9	21.6 28.8 36.0 43.2 50.4 57.6 64.8	14.6 21.9 29.2 36.5 43.8 51.1 58.4 65.7	14.8 22.2 29.6 37.0 44.4 51.8 59.2 66.6	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5	15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	15.4 23.1 30.8 38.5 46.2 53.9 61.6 69.3	15.6 23.4 31.2 39.0 46.8 54.6 62.4 70.2	15.8 23.7 31.6 39.5 47.4 55.3 63.2 71.1	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0	2 3 4 5 6 7 8 9
0.4 7.2 4.0 0.8 7.6 4.4 1.2	20.7 27.6 34.5 41.4 48.3 55.2 62.1	21.0 28.0 35.0 42.0 49.0 56.0 63.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8 63.9	21.6 28.8 36.0 43.2 50.4 57.6 64.8	14.6 21.9 29.2 36.5 43.8 51.1 58.4 65.7	14.8 22.2 29.6 37.0 44.4 51.8 59.2 66.6	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5	15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	15.4 23.1 30.8 38.5 46.2 53.9 61.6 69.3	15.6 23.4 31.2 39.0 46.8 54.6 62.4 70.2	15.8 23.7 31.6 39.5 47.4 55.3 63.2 71.1	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0	2 3 4 5 6 7 8 9
0.4 7.2 4.0 0.8 7.6 4.4 1.2	20.7 27.6 34.5 41.4 48.3 55.2 62.1 8.9 17.8	21.0 28.0 35.0 42.0 49.0 56.0 63.0 90 18.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8 63.9	21.6 28.8 36.0 43.2 50.4 57.6 64.8	14.6 21.9 29.2 36.5 43.8 51.1 58.4 65.7	14.8 22.2 29.6 37.0 44.4 51.8 59.2 66.6	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5 9.5 19.0	15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	15.4 23.1 30.8 38.5 46.2 53.9 61.6 69.3	15.6 23.4 31.2 39.0 46.8 54.6 62.4 70.2	15.8 23.7 31.6 39.5 47.4 55.3 63.2 71.1	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 10.0 20.0	2 3 4 5 6 7 8 9
0.4 7.2 4.0 0.8 7.6 4.4 1.2 8.8 7.6 6.4	20.7 27.6 34.5 41.4 48.3 55.2 62.1 8.9 17.8 26.7	21.0 28.0 35.0 42.0 49.0 56.0 63.0 9.0 18.0 27.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8 63.9	21.6 28.8 36.0 43.2 50.4 57.6 64.8 9.2 18.4 27.6	14.6 21.9 29.2 36.5 43.8 51.1 58.4 65.7	14.8 22.2 29.6 37.0 44.4 51.8 59.2 66.6	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5 9.5 19.0 28.5	15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	15.4 23.1 30.8 38.5 46.2 53.9 61.6 69.3 9.7 19.4 29.1	15.6 23.4 31.2 39.0 46.8 54.6 62.4 70.2 9.8 19.6 29.4	15.8 23.7 31.6 39.5 47.4 65.3 63.2 71.1 9.9 19.8 29.7	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 10.0 20.0 30.0	2 3 4 5 6 7 8 9
0.4 7.2 4.0 0.8 7.6 4.4 1.2 8.8 7.6 6.4 5.2	20.7 27.6 34.5 41.4 48.3 55.2 62.1 8.9 17.8 26.7 35.6	21.0 28.0 35.0 42.0 49.0 56.0 63.0 9.0 18.0 27.0 36.0	14.2 21.3 28.4 35.5 42.6 49.7 56.8 63.9 9.1 18.2 27.3 36.4	21.6 28.8 36.0 43.2 50.4 57.6 64.8 9.2 18.4 27.6 36.8	14.6 21.9 29.2 36.5 43.8 51.1 58.4 65.7 9.3 18.6 27.9 37.2	14.8 22.2 29.6 37.0 44.4 51.8 59.2 66.6 9.4 18.8 28.2 37.6	15.0 22.5 30.0 37.5 45.0 52.5 60.0 67.5 9.5 19.0 28.5 38.0	15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	15.4 23.1 30.8 38.5 46.2 53.9 61.6 69.3 9.7 19.4 29.1 38.8	15.6 23.4 31.2 39.0 46.8 54.6 62.4 70.2 9.8 19.6 29.4 39.2	15.8 23.7 31.6 39.5 47.4 55.3 63.2 71.1 9.9 19.8 29.7 39.6	16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 10.0 20.0 30.0 40.0	2 3 4 5 6 7 8 9
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